

UNCLASSIFIED

AD NUMBER
AD872180
NEW LIMITATION CHANGE
TO Approved for public release, distribution unlimited
FROM Distribution authorized to U.S. Gov't. agencies and their contractors; Critical Technology; APR 1970. Other requests shall be referred to Naval Sea Systems Command, ATTN: AIR-530214, Washington, DC 20360.
AUTHORITY
USNASC ltr dtd 26 Oct 1971

THIS PAGE IS UNCLASSIFIED



COFA II  
COLLOCATION FLUTTER ANALYSIS STUDY II

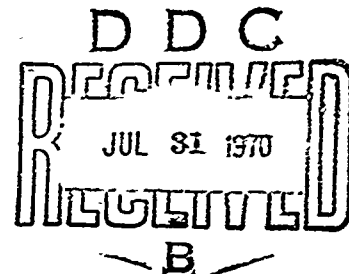
VOLUME II  
UNSTEADY AERODYNAMIC GENERALIZED FORCE PROGRAMS  
FOR SUBSONIC, TRANSONIC, AND SUPERSONIC FLIGHT REGIMES

PREPARED BY DYNAMICS & ENVIRONMENTS SECTION PERSONNEL, HUGHES  
AIRCRAFT COMPANY, MISSILE SYSTEMS DIVISION, CONTRACT NO. 00019-69-C-0427

APRIL 1970

This document is subject to special export controls and transmittal to foreign governments or foreign nationals may be made only with prior approval of the Naval Air Systems Command (AIR-530214).

*Wash, D.C. 20360*



## TABLE OF CONTENTS

Section	Page No.
1.0 Introduction	1
2.0 Unsteady Aerodynamics Generalized Forces	2
3.0 Subsonic Unsteady Aerodynamics Program	4
3.1 Theoretical Derivation	4
3.2 Program Description	7
3.3 Input Instructions	10
3.4 Sample Problem	15
3.5 Program Listing	22
4.0 Transonic Unsteady Aerodynamics Program	38
4.1 Theoretical Derivation	38
4.2 Program Description	41
4.3 Input Instructions	44
4.4 Sample Problem	48
4.5 Program Listing	56
5.0 Supersonic Unsteady Aerodynamics Program	69
5.1 Theoretical Derivation	69
5.2 Program Description	73
5.3 Input Instructions	76
5.4 Sample Problem	80
5.5 Program Listing	88
6.0 References	99

## 1.0 INTRODUCTION

The flutter problem can be solved with either a collocation or normal-mode formulation. The collocation approach is attractive if an accurate stiffness and aerodynamic influence coefficient matrix can be formed for the system. The normal-mode method merits consideration when mode shapes and natural frequencies for the structure are known. The normal-mode method requires the aerodynamics to be presented as generalized forces. The normal-mode formulation is generally presented in the following manner

$$(\bar{M}) + [\bar{Q}] - \frac{1+ig}{\omega^2} [\omega_n^2] [\bar{M}] \{\psi\} = 0$$

Where

$[\bar{M}]$  = Generalized Mass Matrix

$[\bar{Q}]$  = Generalized Aerodynamic Force Matrix

$g$  = Artificial Structural Damping

$i$  =  $\sqrt{-1}$

$\omega$  = Flutter Frequency

$\omega_n$  = Natural Vibration Frequency

$\psi$  = Generalized Coordinate

This volume presents three computer programs that calculate the generalized aerodynamic forces for the three flight regimes: Subsonic Flight, Transonic Flight, Supersonic Flight and may be used with the Modal Flutter Analysis Program of Vol. III. The subsonic program is based upon Kernel Function formulation. The transonic and supersonic programs are based upon the Mach Box technique. (

## 2.0 UNSTEADY AERODYNAMIC GENERALIZED FORCES

The generalized force  $Q_{ij}$  is defined as the work done in mode  $i$  by the pressures due to motion of mode  $j$ . If  $z^i(x,y)$  is the deformation pattern of mode  $i$  and  $\Delta P_j(x,y)$  is the pressure distribution of mode  $j$  then

$$Q_{ij} = \int \int z^i(x,y) \Delta P_j(x,y) dx dy \quad 2.0.1$$

Oscillation of a lifting surface creates a phase lead (or lag) between the pressure and motion of the surface thereby making  $Q_{ij}$  a complex quantity.

The frequency dependency of the generalized force makes the flutter solution a trial and error procedure. Different frequencies must be tried until the flutter frequency and the generalized force frequency coincides. Fortunately, the flutter frequencies are usually near the natural frequencies. This is especially true for a stable structure with modes which remain fairly uncoupled; there is little drifting of oscillatory frequencies with the presence of aerodynamic forces.

Various lifting surface theories were employed to determine the pressure distribution  $\Delta P_j(x,y)$  for generalized force calculations. This was required to correctly account for the high degree of chordwise and spanwise deformation associated with mode shapes of low aspect ratio surfaces. Also, it was necessary to include aerodynamic interaction effects between tandem surfaces.

The methods are based on the linearized equation of fluid motion which describe the flow patterns for a compressible, inviscid, isentropic and irrotational fluid. The boundary conditions are consistent with thin wing theory. The effects of high angles of attack and missile body influence on the aerodynamics of the lifting surfaces were not considered in the analysis.

The linearized equation for time dependent disturbances is

$$\bar{\phi}_{XX} + \bar{\phi}_{YY} + \bar{\phi}_{ZZ} = M^2 \left( \bar{\phi}_{XX} + \frac{2}{U} \bar{\phi}_{XT} + \frac{1}{U} \bar{\phi}_{TT} \right) \quad 2.0.2$$

where  $\bar{\phi}$  is the perturbation velocity potential at the point  $(X, Y, Z)$ .  $M$  and  $U$  are the free stream Mach number and velocity, respectively. Imposing the requirement of harmonic motion, this time dependency can be expressed as

$$\bar{\phi} = b \phi e^{i\omega t}$$

where  $\phi$  is the nondimensional complex amplitude of the velocity potential and  $b$  is a reference semi-chord. The equation may be cast in a nondimensional form by substitution of the following dimensionless parameters:

$$x = X/b$$

$$y = Y/b$$

$$z = Z/b$$

$$k = \omega b/U$$

This yields

$$\phi_{xx} + \phi_{yy} + \phi_{zz} = M^2 (\phi_{xx} + 2ik \phi_x - k^2 \phi)$$

2.0.3

It is this relationship which must be satisfied for  $M < 1$ ,  $M = 1$ , and  $M > 1$ . A brief description of the analytical techniques employed for each speed regime is presented in the following sections. The numerical and computational schemes used are similar to those which are described in detail in References 5, 6, and 7.

### 3.0 SUBSONIC UNSTEADY AERODYNAMICS PROGRAM

#### 3.1 Theoretical Derivation

Subsonic aerodynamic loads were derived by the kernel function method and the resulting loads were then used to compute generalized forces. The subsonic kernel function relationship for the downwash  $(x,y)$  on a surface in terms of the pressure over the entire surface is

$$w(x,y) = -\frac{1}{8\pi} \iint \frac{\Delta P}{1/2\rho U^2} K(x-\xi, y-\eta) d\xi d\eta \quad 3.1.1$$

This relationship is derived by noting that the potential equation for subsonic flow,

$$(1-M^2)\phi_{xx} + \phi_{yy} + \phi_{zz} = M^2 (2ik\phi_x - k^2\phi) \quad 3.1.2$$

is satisfied at  $(x,y,z)$  by the pulsating pressure doublet

$$\phi = -A \frac{\partial}{\partial \xi} e^{-ik(x-\xi)} \int_{-\infty}^{x-\xi} \frac{1}{R'} \exp \left[ \frac{ik}{1-M^2} (\lambda - MR') \right] d\lambda \quad 3.1.3$$

where

$$R' = \sqrt{\lambda^2 + (1-M^2)(y-\eta)^2 + (z-\xi)^2} \quad 3.1.4$$

and the pressure doublet strength is given by

$$A = \frac{1}{4\pi} \left[ \frac{\Delta P(\xi, \eta)}{1/2\rho U^2} \right] d\xi d\eta \quad 3.1.5$$

The velocity normal to the lifting surface is given by

$$w(x,y) = \lim_{z \rightarrow 0} \frac{\partial \phi}{\partial z} \quad 3.1.6$$

Substituting equation (3.1.3) into the equation above and integrating over the area yields the kernel function relationship, equation (3.1.1). For tandem surfaces, the integration extends over both surfaces:

$$w(x,y) = -\frac{1}{8\pi} \int_{-s}^{+s} \int_{1.e.}^{t.e.} \frac{\Delta P_{W(\xi, \eta)}}{1/2\rho U^2} K(x-\xi, y-\eta) d\xi d\eta$$

wing

$$- \frac{1}{8\pi} \int_{-s}^{+s} \int_{1.e.}^{t.e.} \frac{\Delta P_{cs(\xi, \eta)}}{1/2\rho U^2} K(x-\xi, y-\eta) d\xi d\eta$$

control surface

3.1.7



The kernel function at any point is given by

$$K(x-\xi, y-\eta) = \lim_{\substack{\zeta \rightarrow 0 \\ z \rightarrow 0}} \left\{ e^{-ik(x-\xi)} \frac{\partial}{\partial z} \frac{\partial}{\partial \zeta} \int_{-\infty}^{x-\xi} \frac{1}{R'} e^{i \left[ \frac{1}{1-M^2} (\lambda - MR') \right]} d\lambda \right\} \quad (3.1.8)$$

Equation (3.1.7) then represents the integral equation wherein given the downwash  $w(x,y)$  over the wing and control surface,  $\Delta P_w$  and  $\Delta P_{cs}$  must then be determined.

The pressure distribution is approximated as the sum of a series of functions which have the proper behavior as inferred from steady state and two-dimensional solutions. The pressure on each surface can be approximated in the form

$$\Delta P \approx \frac{1}{2} \rho U^2 \frac{\sqrt{s^2 - \eta^2}}{b(\eta)} \sum_{n=0}^N \sum_{m=0}^M a_{nm} P_m(\eta) f_n(\xi) \quad (3.1.9)$$

where

$$\begin{aligned} f_0(\xi) &= \sqrt{\frac{1-\xi}{1+\xi}} & f_n(\xi) &= \sqrt{1-\xi^2} T_{n-1}(\xi); \quad n \geq 1 \\ P_0(\eta) &= 1.0 & P_m(\eta) &= \eta^2 T_{m-1}(\eta); \quad m \geq 1 \end{aligned} \quad (3.1.10)$$

$$T_0(x) = 1.0$$

$$T_1(x) = 2x$$

$$T_k(x) = 2xT_{k-1}(x) - T_{k-2}(x); \quad k \geq 2$$

$$\tilde{\xi} = \frac{\xi - \bar{\xi}}{b(\eta)}$$

$$\tilde{\xi} = 1/2 (\xi_{l.e.} + \xi_{t.e.})$$

$$\underline{\eta} = \frac{\eta}{s}$$

s is the starboard coordinate of the surface tip and  $b(\eta)$  is the local semi-chord. The functions  $T_n$  are Chebyshev polynomials and are introduced for purposes of convenience.

Substituting equation (3.1.8, 3.1.9, and 3.1.10) into equation (3.1.7) yields a set of equations relating the pressure coefficients for the wing,  $a_{nm}^w$ , and the control surface,  $a_{nm}^{cs}$ , to the downwashes. In matrix notation this gives

$$\begin{Bmatrix} \{w^w\} \\ \{w^{cs}\} \end{Bmatrix} = \begin{bmatrix} D_{nm}^{ww} & D_{nm}^{w-cs} \\ D_{nm}^{cs-w} & D_{nm}^{cs} \end{bmatrix} \times \begin{Bmatrix} a_{nm}^w \\ a_{nm}^{cs} \end{Bmatrix} \quad (3.3.11)$$

The integrals involved in evaluating the D's were solved by the methods of Hsu (Reference 5). In this procedure the integrals are numerically evaluated using the Gauss-Mehler quadrature. Upon determining values for the D's, the pressure coefficients are found by direct inversion and the generalized forces are found by application of equation (2.0.1).

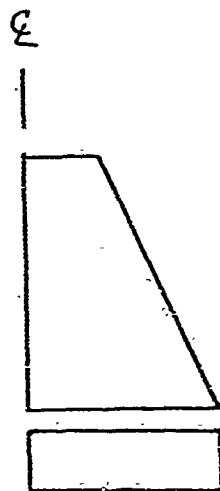
### 3.2 Program Description

The Subsonic Generalized Force Unsteady Aerodynamics Program calculates generalized forces for up to 10 deformation modes. The computer solution, which is based upon the kernel function formulation, is applicable to a variety of configurations. The various configurations which can be analyzed are shown in Figure 3.2.1 and Table 3.2.2. The analysis includes interaction effects between tandem surfaces and wake effects on the trailing surface. The number of integration stations are chosen, and they are automatically located. The collocation stations are then interdigitated between the integration stations, according to Hsu (Reference 5), internally in the program. The solutions at the collocation stations are then matched to terms in the downwash series by a least squares method and the surface pressure are determined. The method of solution programmed does not allow for a single surface to be analyzed separately; however, an option to isolate and eliminate interference effects between the two surfaces is available. Thus, a single surface can be analyzed by using the option ISOLAT and inputting a dummy second surface.

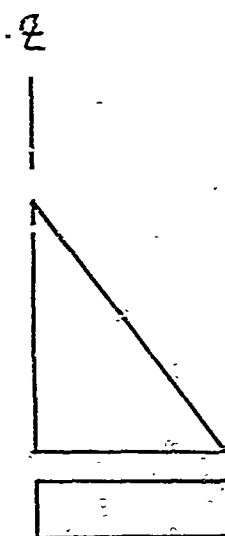
The solution for the generalized aerodynamic forces requires the input of the deformation modes due to vibration. The program considers the modes to be expressed as analytic functions of the form:

$$w(x, y) = \sum_{m=0}^N \sum_{n=0}^n C_{(n-m), m} x^{(n-m)} y^m$$

To meet this requirement only the coefficients "c" are required as input into the program. These coefficients can be obtained in several ways, the most common way is to surface fit the modes by the least-square technique.



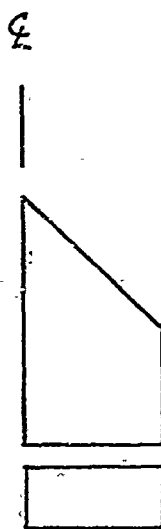
TRAPEZOIDAL



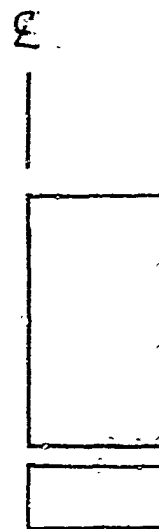
DELTA



TRAPEZOIDAL  
(CROPPED)



DELTA  
(CROPPED)



RECTANGULAR

FIGURE 3.2.1  
TANDEM COPLANAR CONFIGURATIONS AT SUBSONIC  
MACH NUMBER

TABLE 3.2.2 - OPTIONAL CONFIGURATIONS

Configuration	Chordwise Coordinates	Spanwise Coordinates
Rectangular	$X(1) = 0.0$ $X(2) = 0.0$ $X(3) > 0.0$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
Delta	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
Trapezoidal	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
Trapezoidal (Cropped)	$X(1) = 0.0$ $X(2) > X(1)$ $X(3) > X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
Delta (Cropped)	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) > X(2)$ $X(4) > X(3)$ $X(5) > X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > Y(2)$

### 3.3 INPUT INSTRUCTIONS

Instructions for preparing input data for the subsonic computer program are presented here. The field location and format for each input quantity is specified. Any set of units may be used for geometric dimensions and acoustic velocity as long as they are consistent; e.g., if feet is used for length then the acoustic velocity must have dimensions of feet per second.

#### 1. Streamwise Coordinates (6El2.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	X(1)	X(2)	X(3)	X(4)	X(5)	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) X(1) Wing root leading edge streamwise coordinate (See Figure 3.3.1)
- (2) X(2) Wing tip leading edge streamwise coordinate
- (3) X(3) Wing trailing edge streamwise coordinate
- (4) X(4) Control surface leading edge streamwise coordinate
- (5) X(5) Control surface trailing edge streamwise coordinate

The technique for generating various configurations is shown in Table 3.2.1

The origin for the planform and AIC station coordinates must be at the leading edge root of the wing therefore X(1) and Y(1), described below, must always be 0.0.

#### 2. Spanwise Coordinates and Acoustic Velocity (6El2.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	Y(1)	Y(2)	Y(3)	SOUND	RHO	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) Y(1) Wing root spanwise coordinate
- (2) Y(2) Wing leading edge spanwise coordinate
- (3) Y(3) Wing (and control surface) tip spanwise coordinate
- (4) SOUND Acoustic velocity for altitude at which analysis is performed
- (5) RHO density of fluid  $\times 1000.0$  ( $M/L^3$ )

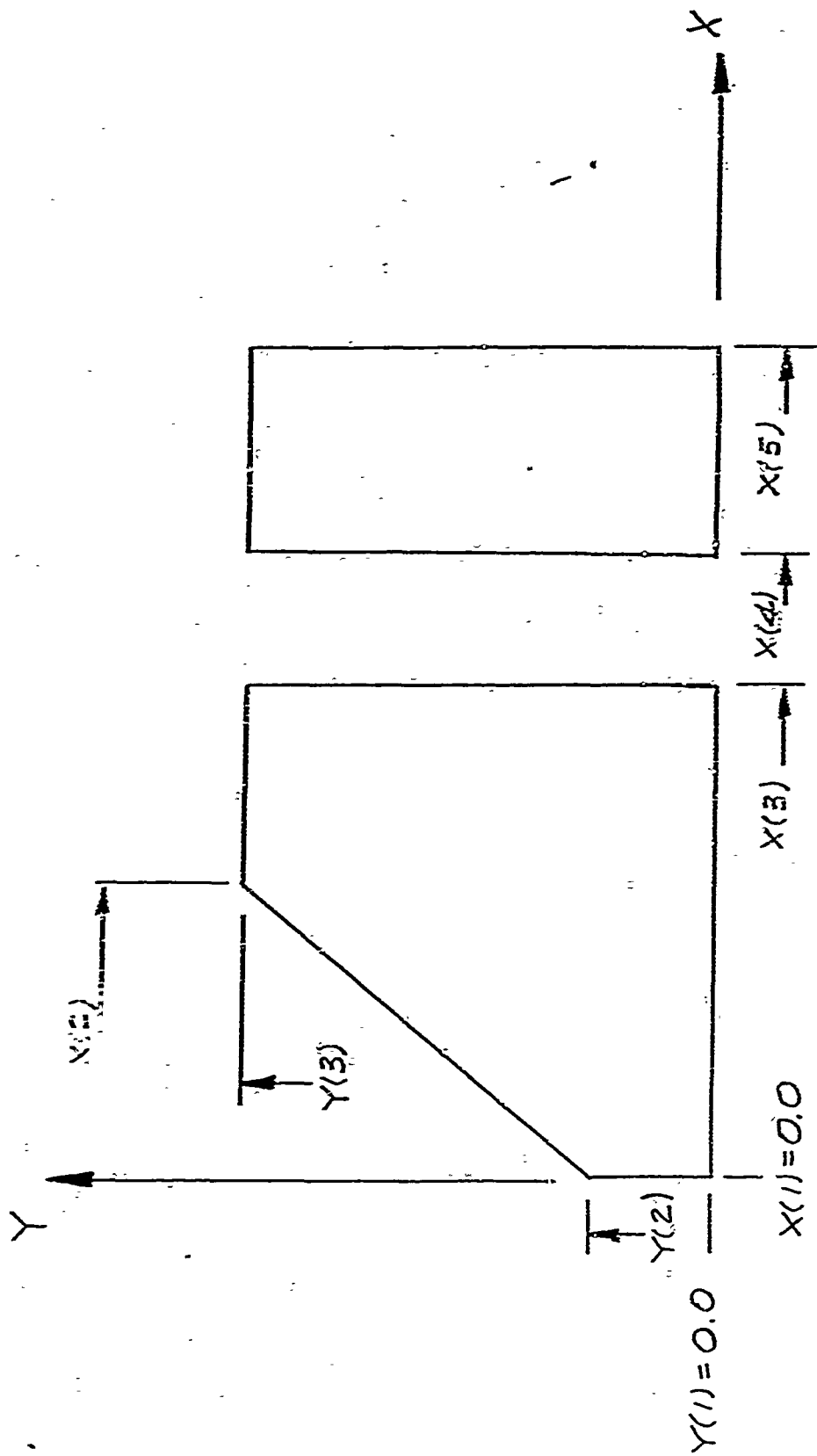


FIGURE 3.3.1  
GEOMETRY DESCRIPTION

### 3. General Information (6112 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NYACH	NFREQ	NMODES	LCOLL	LPRWSH	LPRCØ
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NYACH Number of Mach numbers (max 6)  
 (2) NFREQ Number of frequencies at each Mach number (max 10)  
 (3) NMODES Number of deformation modes (max 10)  
 (4) LCOLL Print collocation stations; 1 ~ Yes; 0 ~ No  
 (5) LPRWSH Print pressures and downwashes; 1 ~ Yes; 0 ~ No  
 (6) LPRCØ Print pressure coefficients; 1 ~ Yes; 0 ~ No

### 4. General Information (6112 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NWCX	NWPX	NCCX	NCPX	NIØNCX	
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NWCX Number of chord collocation stations - wing(max 10)  
 (2) NWPX Number of chord pressure series terms - wing(max 10)  
 (3) NCCX Number of chord collocation stations - control surface(max 10)  
 (4) NCPX Number of chord pressure series terms - control surface(max 10)  
 (5) NIØNCX Choose a value of NIØNCX such that  $NIØNCX \neq (NWCX \text{ or } NCCX)$   
 equals the number of chordwise integration stations  

$$\left( \text{Max } \frac{40}{NWCX} \text{ or } \frac{40}{NCCX} \right)$$

### 5. General Information (6112 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NIY	NWCY	NPY	INWTS	ISØLAT	
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NIY Number of spanwise integration stations (max 11)  
 (2) NWCY Number of spanwise collocation stations - wing (max 11)  
 (3) NPY Number of spanwise pressure series terms (max 10)  
 (4) INWTS Read downwash error weighting factors; 1 ~ Yes; 0 ~ No  
 (5) ISØLAT Isolate wing and control surface; 1 ~ Yes; 0 ~ No

### 6. Weighting Factors (6E12.5 format)(omit these cards when INWTS = 0)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	WT(1)	WT(2)	WT(3)	WT(4)	WT(5)	WT(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

Continue on successive cards until  $WT(i) = WT(NWTS)$   
 Where  $NWTS = NWCY \neq NWCX + NIY \neq NCCX$



7. NØMIT (6I12 format) (omit these cards when NWCY = NIY)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NØM(1)	NØM(2)	NØM(3)	NØM(4)	NØM(5)	NØM(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

Continue on successive cards until  $NØM(i) = NØM(NØMIT)$  where  $NØMIT = NIY - NWCY$ . For the solution to be carried out, NWCY must equal NIY. When an excessive number of collocation stations exist, they must be eliminated by spanwise rows. NØM(i) is the spanwise row number to be eliminated. NØMIT = NIY - NWCY is the number of spanwise rows to be eliminated.

8. Mach Numbers (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FMACH(1)	FMACH(2)	FMACH(3)	FMACH(4)	FMACH(5)	FMACH(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FMACH(1) Mach number  
(2) FMACH(2) Mach number

· · ·  
· · ·  
· · ·  
· · ·

(FMACH) FMACH(NMACH) Mach number

FMACH values of Mach number must be input. Mach numbers must be greater than zero and less than 0.95.

9. Frequencies (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FREQ(1)	FREQ(2)	FREQ(3)	FREQ(4)	FREQ(5)	FREQ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FREQ(1) f(cps)  
(2) FREQ(2) f(cps)

· · ·  
· · ·  
· · ·  
· · ·

(NFREQ) FREQ(NFREQ)

For NFREQ 6, continue input on new card.

Repeat the following cards  $i = 1, \dots, NMODES$

10. Number of Deformation Mode Polynomial Coefficients to be Read for the  $i^{th}$  Mode First Surface

Format (6I12)	
Column	1-12 13-24
Name	NZCØ(1,i)
Item	(1) (2)

(1) NZCØ(1,i) Number of polynomial coefficients to be read for the first surface, the  $i^{th}$  mode.

Format (6E12.5)					
Column	1-12	13-24	25-36	37-48	49-60 61-72
Name	CØ(0,0)	CØ(1,0)	CØ(0,1)	CØ(2,0)	CØ(1,1) CØ(0,2)
Item	(1)	(2)	(3)	(4)	(5) (6)

CØ(i,j) Deformation polynomial coefficients for the first surface in the order: 0,0; 1,0; 0,1; 2,0; 1,1; 2,0; etc. where the first integer is the power of "x" and the second is the power of "y"

Format (6I12)	
Column	1-12 13-24
Name	NZCØ(2,i)
Item	(1) (2)

(1) NZCØ(2,i) Number of polynomial coefficients to be read for the second surface and the  $i^{th}$  mode.

Format (6E12.5)					
Column	1-12	13-24	25-36	37-48	49-60 61-72
Name	CØ(0,0)	CØ(1,0)	CØ(0,1)	CØ(2,0)	CØ(1,1) CØ(0,2)
Item	(1)	(2)	(3)	(4)	(5) (6)

CØ(i,j) Deformation polynomial coefficients for the second surface in the order: 0,0; 1,0; 0,1; 2,0; 1,1; 2,0; etc.; where the first integer is the power of "x" and the second is the power of "y"

### 3.4 SAMPLE PROBLEM

The generalized forces are calculated for the configuration below. The flight parameters and pertinent input data are presented on the first page of the computer print out.

The coefficients of the deformation modes for the forward surface are shown on the second page of the computer print out, and for the aft surface on the third page of the computer print out.

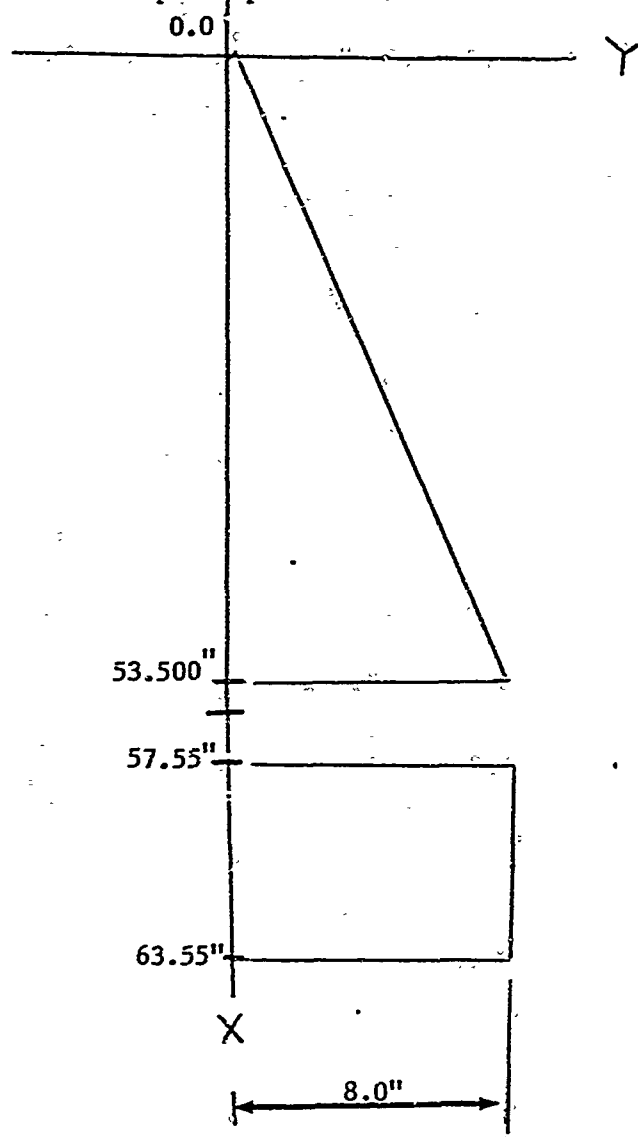


Figure 3.4.1

# HAC/NAA MISSILE SUBSONIC AIRLOADS PROGRAM

## FLIGHT CONDITIONS AND GEOMETRY

MACH NUMBER = 0.75000      SPEED OF SOUND = 13392.000 L/1       $RHO=0.11460000E-06$

	WING	TAIL
L.E. STATION (L)	0.	57.550
ROOT CHORD (L)	53.500	6.000
L.E. SPAN (L)	0.	8.000
T.E. SPAN (L)	8.000	8.000
TIP CHORD (L)	0.	6.000
TOTAL AREA (L*L)	428.000	96.000
SPAN COLL. STA.	5	5
CHORD COLL. STA.	5	4
CHORD INTG. STA.	25	20
SPAN PRES MODES	5	5
CHORD PRES MODES	5	4

# MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 175.00000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92843 FREE STREAM MACH NUMBER 0.750

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR WING  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE	COEFFS.							
1	2.0521E-04	-5.1369E-03	-1.7297E-01	6.6410E-04	1.2377E-02	9.4315E-02	-4.0663E-05	
	3.4901E-04	-1.8280E-02	4.4315E-02	1.0269E-06	-2.7631E-05	7.0302E-04	-2.4386E-03	
	1.7143E-03	-8.7203E-09	3.4448E-07	-7.6417E-06	3.2771E-05	-4.2944E-05	1.4335E-05	
2	-2.0230E-02	6.6160E-03	5.4730E-01	5.5723E-04	-1.2727E-01	1.1243E-01	-1.1355E-04	
	1.1767E-02	-6.1689E-02	2.1984E-01	3.9306E-06	-3.6816E-04	3.0863E-03	-1.4335E-02	
	1.2788E-02	-3.8299E-08	3.5697E-06	-3.7881E-05	2.0408E-04	-3.1845E-04	1.9772E-04	
3	-8.8265E-03	1.5226E-03	-1.3938E 00	2.2485E-03	1.2298E-01	6.1586E-01	-2.4958E-04	
	2.5723E-03	-1.2793E-01	3.4273E-01	7.6501E-06	-2.4579E-04	5.1801E-03	-1.9536E-02	
	1.3232E-02	-7.0887E-08	3.0849E-06	-5.6882E-05	2.4816E-04	-2.3222E-04	-7.4070E-05	
4	-2.3616E-03	-9.5670E-03	-1.2947E-01	8.8089E-04	2.8617E-02	5.8725E-02	-4.8745E-05	
	7.3151E-04	-5.9538E-02	2.1428E-01	1.1771E-06	-5.9277E-05	2.1117E-03	-6.0253E-03	
	-9.4423E-03	-0.8432E-09	6.9796E-07	-1.9536E-05	4.5021E-05	1.1500E-04	1.5178E-04	
5	-1.8034E-04	-1.8284E-05	1.3879E-02	-1.0982E-05	-2.9642E-03	-3.9850E-04	7.7560E-07	
	1.4335E-04	3.0570E-04	-9.9055E-04	-1.6682E-08	-3.5623E-06	1.1936E-06	-5.9706E-05	
	2.6742E-04	1.1484E-10	3.0569E-08	-1.4258E-07	2.1170E-06	-1.1500E-05	1.9655E-05	

17

# MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GHS) 175.00000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92043 FREE STREAM MACH NUMBER 0.750

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR TAIL  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION.

MODE	COEFFS.						
1	-2.5045E-01 -5.1564E-04 2.6874E-04	1.3407E-02 8.8247E-04	-2.0109E-02 -1.6279E-03	9.0702E-04 3.9499E-05	-1.5111E-03 4.6416E-05	-1.3471E-02 1.1246E-06	-4.2571E-04 -5.2663E-05
2	-6.0722E-02 -4.4974E-04 -2.5385E-05	1.3622E-02 2.4416E-05	-5.0481E-03 2.8156E-04	-5.7007E-03 -1.5632E-04	1.1958E-03 4.2814E-05	-1.3226E-03 8.0306E-06	1.7453E-03 3.5725E-06
3	-1.6215E-02 4.4260E-05 -2.1265E-05	1.1602E-02 1.9642E-04	7.1003E-03 2.5398E-04	3.8815E-04 3.4503E-05	-1.5586E-03 -2.3779E-05	8.7454E-05 3.0552E-05	-2.9670E-04 -3.5626E-05
4	1.4420E-01 -8.4577E-03 -1.3343E-04	-2.2355E-01 -1.4563E-03	-3.9674E-02 -2.6337E-05	9.4683E-02 1.0735E-03	3.2691E-02 7.1000E-04	1.8561E-02 1.5943E-04	-1.7439E-02 -1.6472E-06
5	-6.0398E-01 -3.2443E-03 -4.9674E-05	3.1261E-01 6.1969E-04	-1.2775E-02 9.6992E-04	-4.3907E-02 -8.0275E-04	1.2655E-02 3.4466E-04	-4.9283E-03 3.4043E-04	9.3476E-03 -1.8608E-04

# MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GHS) 175.00000 5 DEFLECTION MODES

REDUCED FREQUENCY (SEMI CHORD) 2.92843 FREE STREAM MACH NUMBER 0.750

## GENERALIZED FORCES FOR WING

DEFI	LOAD	REAL PART	IMAG PART	AHS VALUE	PHASE ANGLE
1	1	1.78433E 00	-1.20375E-01	2.78839E 00	-3.859 DEG
1	2	-4.19576E 00	1.94784E 00	-4.62580E 00	155.097 DEG
1	3	9.34031E-01	-1.27098E 01	1.27441E 01	-85.797 DEG
1	4	1.03725E 01	6.67475E 00	1.23345E 01	32.762 DEG
1	5	-5.40024E-02	6.39892E-01	6.42167E-01	94.824 DEG
2	1	-7.67248E 00	-2.67310E 00	8.12480E 00	-160.792 DEG
2	2	1.58403E 01	-6.01938E 00	1.69455E 01	-20.807 DEG
2	3	-2.68136E 01	3.93086E 01	4.75829E 01	124.299 DEG
2	4	-2.46347E 01	-3.70716E 01	4.45103E 01	-123.605 DEG
2	5	8.50254E 00	-9.48398E 00	1.27373E 01	-48.123 DEG
3	1	4.08041E 00	2.08681E 01	-2.12633E 01	78.936 DEG
3	2	1.35203E 01	-2.18268E 01	2.56735E 01	-58.225 DEG
3	3	1.99015E 02	-7.14507E 00	1.99143E 02	-2.056 DEG
3	4	-9.86493E 01	1.51302E 02	1.88621E 02	123.104 DEG
3	5	-2.47112E 01	3.74600E 01	4.48771E 01	123.411 DEG
4	1	6.04738E 00	-1.57318E 01	1.68541E 01	-68.597J DEG
4	2	-3.81082E 01	2.17331E 01	4.38699E 01	150.304 DEG
4	3	-1.44431E 02	-7.27240E 01	1.61707E 02	-153.274 DEG
4	4	1.36556E 02	-6.84736E 01	1.52762E 02	-26.631 DEG
4	5	1.99313E 01	-3.89072E 01	3.67765E 01	-57.183 DEG
5	1	-1.62374E-01	-9.08498E-02	1.86062E-01	-350.77J DEG
5	2	2.19044E-01	2.21553E-01	3.11554E-01	45.326 DEG
5	3	-9.80154E-01	1.64998E 00	1.87955E 00	118.615 DEG
5	4	-6.57931E-01	-1.65552E 00	1.78147E 00	-111.674 DEG
5	5	1.48400E-03	-2.23596E-01	2.23604E-01	-89.620 DEG

# MISSILE SUBSONIC AIRPLAUS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 175.00000 5 DEFLECTION MODES

REDUCED FREQUENCY (SP-MI CHORD) 2.92643 FREEL STREAM MACH NUMBER 0.750

## GENERALIZED FORCES FOR TAIL

DEFL	LOAD	REAL PART	IMAG PART	AUS VALUE	PHASE ANGLE
1	1	1.68414E 01	-2.35843E 01	2.89802E 01	-54.470 DEU
1	2	-2.64020E 01	8.04695E 00	2.76019E 01	163.050 DEU
1	3	1.10991E 02	9.07857E 01	1.43392E 02	39.282 DEU
1	4	-1.18089E 02	1.10429E 01	1.18000E 02	174.857 DEU
1	5	9.33634E 01	4.66232E 01	1.04357E 02	26.536 DEU
2	1	1.08962E 00	-3.90206E 00	4.05134E 00	-74.390 DEU
2	2	-3.30264E 00	1.10511E 00	3.50889E 00	160.260 DEU
2	3	1.04867E 01	1.49847E 01	1.82097E 01	55.015 DEU
2	4	-1.60185E 01	-2.94656E 00	1.70746E 01	-170.063 DEU
2	5	1.51049E 01	-1.46806E 02	1.51049E 01	-0.056 DEU
3	1	-1.75394E 00	8.69312E 01	1.95755E 00	153.635 DEU
3	2	1.67228E 00	-5.61288E 01	1.77043E 00	-19.168 DEU
3	3	-9.53124E 00	-2.84436E 00	9.94660E 00	-163.384 DEU
3	4	5.84635E 00	-4.02413E 00	7.09660E 00	-34.545 DEU
3	5	-3.34095E 00	-6.99428E 00	7.75125E 00	-115.532 DEU
4	1	-7.04105E 00	9.89088E 00	1.21411E 01	125.446 DEU
4	2	8.45155E 00	3.31607E 01	8.45920E 00	2.450 DEU
4	3	-4.93566E 01	-2.94018E 01	5.74584E 01	-149.218 DEU
4	4	4.77750E 01	-1.16789E 01	4.91810E 01	-13.737 DEU
4	5	-4.49855E 01	-1.79246E 01	4.84250E 01	-158.275 DEU
5	1	-9.85154E 00	-3.42133E 01	3.56034E 01	-106.063 DEU
5	2	-9.00265E 00	-2.54141E 00	9.35449E 00	-164.236 DEU
5	3	1.16454E 01	9.67320E 01	9.74304E 01	83.135 DEU
5	4	-1.00822E 02	-5.30842E 01	1.13943E 02	-152.233 DEU
5	5	1.42165E 02	-9.58511E 01	1.71459E 02	-33.989 DEU



# MISSILE SUBSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 175.00000 5 DEFLECTION MODES  
 REDUCED FREQUENCY (SEMI CHORD) 2.92843 FREEL STREAM MACH NUMBER 0.750

## GENERALIZED FORCES FOR WING + TAIL

DEFL	LOAD	REAL PART	IMAG PART	AHS VALUE	PHASE ANGLE
1	1	1.86250E 01	-2.37847E 01	3.01408E 01	-51.842 DEG
1	2	-3.05966E 01	9.99479E 00	3.21896E 01	161.911 DEG
1	3	1.11925E 02	7.80759E 01	1.36467E 02	34.899 DEG
1	4	-1.07712E 02	1.7176E 01	1.09160E 02	170.659 DEG
1	5	9.33094E 01	4.72631E 01	1.04597E 02	26.863 DEG
2	1	-6.58286E 00	-6.57516E 00	9.38412E 00	-135.034 DEG
2	2	1.25177E 01	-4.68428E 00	1.34374E 01	-21.886 DEG
2	3	-1.63268E 01	5.42933E 01	5.66951E 01	106.737 DEG
2	4	-4.14532E 01	-4.60181E 01	5.76178E 01	-136.889 DEG
2	5	2.16074E 01	-9.49866E 00	2.54467E 01	-21.918 DEG
3	1	2.32647E 00	2.17374E 01	2.18616E 01	83.821 DEG
3	2	1.51926E 01	-2.24881E 01	2.78728E 01	-55.063 DEG
3	3	1.89483E 02	-9.98943E 00	1.89747E 02	-3.018 DEG
3	4	-9.28040E 01	1.47278E 02	1.74078E 02	122.216 DEG
3	5	-2.80521E 01	3.04665E 01	4.14141E 01	132.637 DEG
4	1	-9.93673E-01	-5.84895E 00	5.92487E 00	-99.655 DEG
4	2	-2.96967E 01	2.20948E 01	3.68824E 01	143.313 DEG
4	3	-1.93708E 02	-1.82126E 02	2.19051E 02	-152.211 DEG
4	4	1.84331E 02	-8.01525E 01	2.01884E 02	-23.581 DEG
4	5	-2.50541E 01	-4.68318E 01	5.48840E 01	-117.161 DEG
5	1	-1.00139E 01	-3.43842E 01	3.57359E 01	-106.823 DEG
5	2	-8.78360E 00	-2.31966E 00	9.08479E 00	-165.285 DEG
5	3	1.07453E 01	9.83820E 01	9.89670E 01	83.767 DEG
5	4	-1.01480E 02	-5.47397E 01	1.15303E 02	-151.657 DEG
5	5	1.42167E 02	-9.60747E 01	1.71586E 02	-34.850 DEG

# 3.5 PROGRAM LISTING

S	OPTION FORTRAN	SUB78020
S	FORTRAN HLSTOU,DECK	SUB78030
S	INCODE IBMF	SUB78038
	CHAIN MAIN	SUB780340
	COMPLEX A,AA,ANH,CZERO,GFORC,DELP,WASH,APR,DWASH,CWASH,PR	SUB780350
	DIMENSION DWASH(90,10),PR(90,10),CWASH(90,10)	SUB780360
	DIMENSION GFORC(10,10,3),DELP(10),WASH(10)	SUB780370
	COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO	SUB780380
	COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNS	SUB780390
	COMMON/C3/NPY,SOUND,NHACH,FHACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB780400
	COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IIY,IIIX,NSURF,ISOLAT	SUB780410
	COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HCOR(6),ZCOR(6),MACH	SUB780420
	COMMON/C6/WXCHN(11),WHCHN(11),WHIN(11),WT(90),XCOLL,YCOLL,PI,U	SUB780430
	COMMON/C7/CO(10,20,2),NZCO(10,2),EM,EK,H2,NWIX,NCIX,WBO,CBOM,NWCY	SUB780440
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB780450
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXHN	SUB780460
	COMMON/CPR/APR(90,60),IMOD,IRON	SUB780470
	EQUIVALENCE (GFORC,AA),(A,WASH),(WASH,DELP)	SUB780480
	EQUIVALENCE (DWASH(1,1),APR(1,51)),(PR(1,1),APR(1,11))	SUB780490
	EQUIVALENCE (CWASH(1,1),APR(1,41))	SUB780500
	WRITE(6,66)	SUB780510
66	FORMAT(1H1)	SUB780520
1	CALL KFDA	SUB780530
	FA = 2*NWIX + 1	SUB780540
	FC = 2*NCIX + 1	SUB780550
	QWXX = 2.0*PI/FW	SUB780560
	QWCX = 2.0*PI/FC	SUB780570
	QWY = PI/FLUAT(2*NIY)	SUB780580
	CALL GEON	SUB780590
	DO 100 MACH=1,NHACH	SUB780600
	MACH = MACH	SUB780610
	EM = FHACH(MACH)	SUB780620
	CALL KOUT(1)	SUB780630
	U = EM*SOUND	SUB780640
	IF(LCOLL.NE.0) CALL KOUT(2)	SUB780650
	ROU = WBO/U	SUB780660
	H2 = 1.0 - EM*EM	SUB780670
	DO 100 IFR=1,NFREQ	SUB780680
	IFR = IFR	SUB780690
	EK = 2.0*PI*FREQ(IFR)*ROU	SUB780700
C	NSURF = 1 (WING) OR 2 (CONTROL)	SUB780710
	NCX = NWCX	SUB780720
	NOMIT = 1	SUB780730
	MAUG = NCOLS + NMODES	SUB780740
	DO 4 J=1,NCOLS	SUB780750
	IL(J) = 0	SUB780760
	DO 4 K=1,MAUG	SUB780770
4	AA(J,K) = CZERO	SUB780780
	IRON = 1	SUB780790
	DO 15 NSURF=1,2	SUB780800
	NSURF = NSURF	SUB780810
	CALL KOUT(6)	SUB780820
C	KOUT (6) PRINTS COEFFICIENTS OF DEFLECTION SERIES	SUB780830
	DO 14 IY=1,NIY	SUB780840
	IIY = IY	SUB780850
	IF(NOMIT-NOMIT.LT.0) GO TO 7	SUB780860
	IF(IY-NOM(NOMIT).EQ.0) GO TO 13	SUB780870
7	YCOLL = SN*Y(IY)	SUB780880
	DO 12 IX=1,NCX	SUB780890
	IIIX = IX	SUB780900

	XCOLL = XS(1,NSURF,IX,IY)	SUB70910
	CALL CORD	SUB70920
C	*** CORD FILLS OUT A ROW OF THE DOWNWASH MATRIX EACH TIME CALLED	SUB70930
	DO 50 M = 1,NMODES	SUB70940
	CALL ZBZX(M,SLOPE,DEFL)	SUB70950
	MNC = NCOLS + M	SUB70960
50	WASH(MNC) = CMPLX(SLOPE,DEFL*EK/WBO)	SUB70970
	DO 40 K=1,MAUG	SUB70980
	K1 = K	SUB70990
	IF(X.GT.NCOLS) K1 = 50 + K - NCOLS	SUB71000
40	APR(IROW,K1) = A(K)	SUB71010
	DO 60 N=1,NCOLS	SUB71020
60	CALL CGRED(A,M,N)	SUB71030
	DO 70 L=1,NMODES	SUB71040
	ML = NCOLS + L	SUB71050
70	ALPHA(L) = SQRT(ALPHA(L)**2 + CABS(A(ML))**2)	SUB71060
	IROW = IROW + 1	SUB71070
12	CONTINUE	SUB71080
	GO TO 14	SUB71090
13	MOMIT = MOMIT + 1	SUB71100
14	CONTINUE	SUB71110
	NCX = NCCX	SUB71120
15	CONTINUE	SUB71130
	CALL XLSQ	SUB71140
C	*****	SUB71150
	IF(LPRCO.EQ.0) GO TO 17	SUB71160
C	*****	SUB71170
	DO 16 IMOD=1,NMODES	SUB71180
	IMOD = IMOD	SUB71190
16	CALL KOUT(3)	SUB71200
C	KOUT(3) PRINTS COEFFICIENTS OF PRESSURE SERIES FOR EACH MODE	SUB71210
C	*****	SUB71220
17	IF(LPRWSH.EQ.0) GO TO 69	SUB71230
C	*****	SUB71240
C	COMPUTE AND STORE THE PRESSURE DOWNWASHES	SUB71250
	MOMIT = 1	SUB71260
	IROW = 1	SUB71270
	NCX = NCCX	SUB71280
	DO 115 NSURF=1,2	SUB71290
	DO 114 IY=1,NIY	SUB71300
	IF(MOMIT.LT.MOMIT) GO TO 107	SUB71310
	IF(IY.EQ.NOM(MOMIT)) GO TO 113	SUB71320
107	DO 112 IX=1,NCX	SUB71330
	DO 140 IM=1,NMODES	SUB71340
	A(IM) = CZERO	SUB71350
	DO 140 JC=1,NCOLS	SUB71360
140	A(IM) = A(IM) + APR(IROW,JC)*ANH(JC,IM)	SUB71370
	DO 150 IM=1,NMODES	SUB71380
150	CHASH(IROW,IM) = A(IM)	SUB71390
	IROW = IROW + 1	SUB71400
112	CONTINUE	SUB71410
	GO TO 114	SUB71420
113	MOMIT = MOMIT + 1	SUB71430
114	CONTINUE	SUB71440
	NCX = NCCX	SUB71450
115	CONTINUE	SUB71460
		SUB71470
C	69 CALL FORC(NWIX,NCIX,NIY,ETA,SIX,WBIN,0)	SUB71480
	IF(LPRWSH.EQ.0) GO TO 77	SUB71490
	CALL FORC(NWCX,NCCX,NIY,Y,SCX,WBCN,LPRWSH)	SUB71500
	DO 99 IMOD=1,NMODES	SUB71510

```

IMOD = IMOD
NCX = NCX
MOMIT = 1
IROW = 1
DO 99 NSURF=1,2
NSURF = NSURF
CALL KOUT (7)
C KOUT (7) PRINTS THE HEADER FOR THE PRESSURE AND DOWNWASH ARRAYS
90 DO 98 IY=1,NIY
IF(NOMIT.LT.MOMIT) GO TO 91
IF(IY.EQ.NOM(MOMIT)) GO TO 97
91 YCOLL = WBO*SN*Y(IY)
DO 96 IX=1,NCX
XCOLL = WBO*XS(1,NSURF,IX,IY)
CALL KOUT(9)
C KOUT (9) PRINTS THE X AND Y COORDINATES OF EACH COLLOCATION
C POINT, THE LOCAL PRESSURE, THE DOWNWASH CREATED THERE BY THE
C PRESSURE FIELD, AND THE DOWNWASH OF THE SURFACE AT THE POINT.
C THE DEGREE TO WHICH THE TWO SETS OF DOWNWASHES MATCH IS A MEASURE
C OF THE ACCURACY OF THE SOLUTION OF THE BOUNDARY VALUE PROBLEM.
C THE ROOT-MEAN-SQUARE OF THE ERRORS IS GIVEN IN THE ARRAY ALPHA.
96 IROW = IROW + 1
GO TO 98
97 MOMIT = MOMIT + 1
98 CONTINUE
NCX = NCCX
99 CONTINUE
C *****
77 DO 78 L=1,3
NSURF = L
78 CALL KOUT(8)
C KOUT(8) PRINTS THE GENERALIZED FORCES
100 CONTINUE
GO TO 1
END
$
$
CCONS1 CONS1
BLOCK DATA
COMPLEX A,AA,ANH,CZERO
COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,MIONCX,RHO
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IY,IIX,NSURF,ISOLAT
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HGOR(6),ZCOR(6),MACH
COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U
COMMON/C7/CO(10,28,2),NZCO(10,2),EH,EK,E2,NWIX,NCIX,WBO,CBON,NWCY
COMMON/C8/IFR,XE(5),YE(5),UX(10),UY(10),WXIMN(11),E1,E2
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWX,QWCX,CXMN
DATA PI/3.14159265/
DATA HGOR/0.08566225,0.18038079,0.23395697,0.23395697,0.18038079,
10.08566225/
DATA ZCOR/0.05376524,0.16939531,0.38069041,0.61930959,0.83060469,
10.96623476/
C *****
C NGSKRN SHOULD BE COMPATIBLE WITH HKER AND ZKER LISTS.
DATA NGSKRN/8/
DATA (HKER(I),I=1,8)/0.05061427,0.11119052,0.15685332,0.18134189
X,0.18134189,0.15685332,0.11119052,0.05061427/
DATA (ZKER(I),I=1,8)/0.01985507,0.10166676,0.23723380,0.40828268
X,0.59171732,0.76276620,0.89833324,0.98014493/

```

```

SUB71520
SUB71530
SUB71540
SUB71550
SUB71560
SUB71570
SUB71580
SUB71590
SUB71600
SUB71610
SUB71620
SUB71630
SUB71640
SUB71650
SUB71660
SUB71670
SUB71680
SUB71690
SUB71700
SUB71710
SUB71720
SUB71730
SUB71740
SUB71750
SUB71760
SUB71770
SUB71780
SUB71790
SUB71800
SUB71810
SUB71820
SUB71830
SUB71840
SUB71850
SUB71860
SUB70030
SUB70040
SUB70050
SUB70060
SUB70070
SUB70080
SUB70090
SUB70100
SUB70110
SUB70120
SUB70130
SUB70140
SUB70150
SUB70160
SUB70170
SUB70180
SUB70190
SUB70200
SUB70210
SUB70220
SUB70230
SUB70240
SUB70250
SUB70260
SUB70270
SUB70280

```

C	*****	SUB70290
	DATA E1/8.0000001/,E2/8.0090001/,CZERO/(0.0,0.0)/	SUB70300
	END	SUB70310
S	FORTRAN NLSTOU,DECK	SUB71870
S	INCODE IBMF	SUB71880
CKFDA	KFDA	SUB71890
	SUBROUTINE KFDA	SUB71900
	COMPLEX A,AA,ANH,CZERO	SUB71910
	COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO	SUB71920
	COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNS	SUB71930
	COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,MIONCX,RHO	SUB71940
	COMMON/C4/NMODES,LCOLL,LPRMSH,LPRCO,NOM(5),I1Y,I1X,MSURF,ISOLAT	SUB71950
	COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HGOR(6),ZGOR(6),MACH	SUB71960
	COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WT(99),XCOLL,YCOLL,P1,U	SUB71970
	COMMON/C7/CU(10,28,2),NZCO(10,2),EM,EK,H2,NWIX,NCIX,WBO,CBON,NWCY	SUB71980
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB71990
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN	SUB72000
	READ(5,11)(XE(I),I=1,5)	SUB72010
	READ(5,11)(YE(I),I=1,3),SOUND,RHO	SUB72020
	RHO = RHO/1000.0	SUB72030
	READ(5,12) NMACH,NFREQ,NMODES,LCOLL,LPRMSH,LPRCO	SUB72040
	READ(5,12) NWCX,NWPX,NCCX,NCPX,MIONCX	SUB72050
	READ(5,12) NIY,NWCY,NPY,INWTS,ISOLAT	SUB72060
	NWTS = NWCY*NWCX + NIY*NCCX	SUB72070
	DO 40 I=1,NWTS	SUB72080
40	WI(I) = 1.0	SUB72090
	IF(INWTS.NE.0) READ(5,11)(WI(I),I=1,NWTS)	SUB72100
	NCOLS = NPY * (NWPX + NCPX)	SUB72110
	NCIX = NCCX*MIONCX	SUB72120
	NWIX = NWCX*MIONCX	SUB72130
	NOMIT = 0	SUB72140
	DO 4 I=1,5	SUB72142
4	NOM(I) = 0	SUB72144
	IF(NWCY.GE.NIY) GO TO 5	SUB72150
	NOMIT = NIY-NWCY	SUB72160
	READ(5,12)(NOM(I),I=1,NOMIT)	SUB72170
5	READ(5,11)(FMACH(I),I=1,NMACH)	SUB72180
	DO 7 I=1,NMACH	SUB72190
	IF(FMACH(I).LE.0.99) GO TO 7	SUB72200
	WRITE(6,13)	SUB72210
13	FORMAT(71H A MACH NUMBER GREATER THAN 0.99 HAS BEEN READ IN---	SUB72220
	1CASE TERMINATED)	SUB72230
	CALL EXIT	SUB72240
7	CONTINUE	SUB72250
	READ(5,11)(FREQ(I),I=1,NFREQ)	SUB72260
	DO 20 I = 1,NMODES	SUB72270
	DO 20 L = 1,2	SUB72280
	DO 10 K = 1,28	SUB72290
10	CU(I,K,L) = 0.0	SUB72300
	READ(5,12) NCO	SUB72310
	NZCU(I,L) = NCO	SUB72320
20	READ(5,11)(CU(I,K,L),K=1,NCO)	SUB72330
	DO 30 I=2,5	SUB72340
30	XE(I) = XE(I) - XE(1)	SUB72350
	YE(2) = YE(2) - YE(1)	SUB72360
	YE(3) = YE(3) - YE(1)	SUB72370
11	FORMAT(6E12.8)	SUB72380
12	FORMAT(6I12)	SUB72390
	IF(NCIX.GT.40.OR.NWIX.GT.40) GO TO 86	SUB72400
	IF(NWCX*NWCY+NCCX*NIY.GT.90) GO TO 86	SUB72410
	IF(NPY*(NWPX+NCPX).GT.50) GO TO 86	SUB72420

	IF(NWPX.GT.10.OR.NCPX.GT.10.OR.NPY.GT.10) GO TO 86	SUB72430
	RETURN	SUB72440
86	EM = FMACH(1)	SUB72450
	CALL KOUT(1)	SUB72460
	CALL KOUT(5)	SUB72470
	RETURN	SUB72480
	END	SUB72490
S	FORTRAN NLSTOU,DECK	SUB72500
S	INCODE IBMF	SUB72510
CGEOM	GEOM	SUB72520
	SUBROUTINE GEOM	SUB72530
	COMPLEX A,AA,ANH,CZERO	SUB72540
	COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO	SUB72550
	COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN	SUB72560
	COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB72570
	COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NUN(5),IIX,IIX,NSURF,ISOLAT	SUB72580
	COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HCO(6),ZCO(6),HACH	SUB72590
	COMMON/C6/WXCHN(11),WBCN(11),WBN(11),WT(90),XCOLL,YCOLL,PI,9	SUB72600
	COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,H2,NWIX,NCIX,WBO,CBON,NWCY	SUB72610
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIHN(11),E1,E2	SUB72620
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXHN	SUB72630
C	WBO = WING ROOT SEMI-CHORD	SUB72640
C	S = SEMI-SPAN	SUB72650
C	WTCN = WING TIP CHORD - NORMALIZED ON WBO	SUB72660
C	WLEN = WING TIP L.E. - NORMALIZED	SUB72670
C	SN = SEMI-SPAN - NORMALIZED	SUB72680
C	CBN = CONTROL SEMI-CHORD	SUB72690
C	FW = 2*NWIX+1	SUB72700
C	FC = 2*NCIX+1	SUB72710
	WBO = XE(3)/2.0	SUB72720
	CLEN = XE(4)/WBO	SUB72730
	S = YE(3)	SUB72740
	WTCN = (XE(3)-XE(2))/WBO	SUB72750
	WLEN = XE(2)/WBO	SUB72760
	SN = S/WBO	SUB72770
	CBN = (XE(5)-XE(4))/2.0	SUB72780
	F1=FW	SUB72790
	F2 = F1*PI/2.	SUB72800
	J = NWIX	SUB72810
C	COMPUTE CHORDWISE INTEGRATION AND COLLOCATION STATIONS	SUB72820
C	FIRST ON THE WING SURFACE	SUB72830
	DO 5 I=1,NWIX	SUB72840
	F2 = F2 -2.*PI	SUB72850
	SIX(J,1) = SIN(F2/F1)	SUB72860
	I1 = FLOAT(I)/FLOAT(NIONCX) + 0.99	SUB72870
	SCX(I1,1) = -SIX(J,1)	SUB72880
5	J=J-1	SUB72890
	F1=FC	SUB72900
	F2 = F1*PI/2.	SUB72910
	J = NCIX	SUB72920
C	THEN ON THE CONTROL SURFACE	SUB72930
	DO 6 I=1,NCIX	SUB72940
	F2 = F2 -2.*PI	SUB72950
	SIX(J,2) = SIN(F2/F1)	SUB72960
	I1 = FLOAT(I)/FLOAT(NIONCX) + 0.99	SUB72970
	SCX(I1,2) = -SIX(J,2)	SUB72980
6	J=J-1	SUB72990
	F1 = 4*NIY	SUB73000
	F2=0.0	SUB73010
C	COMPUTE SPANWISE INTEGRATION AND COLLOCATION STATIONS	SUB73020

DO 8 I=1,NIY	SUB73030
Y(I) = SIN(F2/F1)	SUB73040
F2 = F2 +PI	SUB73050
ETA(I) = SIN(F2/F1)	SUB73060
8 F2 = F2 +PI	SUB73070
C COMPUTE WING SEMI-CHORDS AND MID-CHORD LOCATIONS AT THE	SUB73080
C SPANWISE COLLOCATION AND INTEGRATION STATIONS	SUB73090
PIB = YE(2)/YE(3)	SUB73100
POB =1.0-PIB	SUB73110
CBON = (XE(5)-XE(4))/(2.0*WBO)	SUB73120
CXMN = CBON +XE(4)/WBO	SUB73130
DO 16 I=1,NIY	SUB73140
IF(ETA(I).LE.PIB) GO TO 12	SUB73150
F1 = WLEN*(ETA(I)-PIB)/POB	SUB73160
IF(Y(I).LE.PIB) GO TO 13	SUB73170
F2 = WLEN*(Y(I)-PIB)/POB	SUB73180
GO TO 14	SUB73190
12 F1 = 0.0	SUB73200
13 F2 = 0.0	SUB73210
14 WBIN(I) = 0.5*(2.0-F1)	SUB73220
WXIMN(I) = WBIN(I) +F1	SUB73230
WBCN(I) = 0.5*(2.0-F2)	SUB73240
16 WXCHN(I) = WBCN(I) +F2	SUB73250
36 RETURN	SUB73260
END	SUB73270
FORTRAN NLSTOU,DECK	SUB73280
INCODE IBMF	SUB73290
CXS XS	SUB73300
FUNCTION XS(L,NS,13,J3)	SUB73310
COMPLEX A,AA,ANH,CZERO	SUB73320
COMMON/C1/A(60),A(50,60),ANH(50,10),CZERO	SUB73330
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNS	SUB73340
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB73350
COMMON/C4/NMODFS,LCOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT	SUB73360
COMMON/C5/FW,FC,NCOIS,NOMIT,ALPHA(10),I1(50),HGOR(6),ZCOR(6),MACH	SUB73370
COMMON/C6/WXCHN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U	SUB73380
COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,R2,NWIX,NCIX,WBO,CBON,NWCY	SUB73390
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB73400
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWNX,QWCX,CXMN	SUB73410
GO TO (10,40),L	SUB73420
10 GO TO (20,30),NS	SUB73430
20 XS = WXCHN(J3) + WBCN(J3) * SCX(13,1)	SUB73440
RETURN	SUB73450
30 XS = CXMN + CBON * SCX(13,2)	SUB73460
RETURN	SUB73470
40 GO TO (50,60),NS	SUB73480
50 XS = WXIMN(J3) + WBIN(J3) * SIX(13,1)	SUB73490
RETURN	SUB73500
60 XS = CXMN + CBON * SIX(13,2)	SUB73510
RETURN	SUB73520
END	SUB73530
FORTRAN NLSTOU,DECK	SUB73540
INCODE IBMF	SUB73550
CBESL RESL	SUB73560
FUNCTION BESL(X)	SUB73570
IF(X.GT.2.0) GO TO 50	SUB73580
T=X/3.75	SUB73590
T=T*T	SUB73600
RS11=0.5+T*(0.87890594+T*(0.51498869+T*(0.15084934+T*(0.02658733+T	SUB73610
1*(0.00301532+T*(0.00032411))))))	SUB73620
RS11=RS11*X	SUB73630

	Y=X/2.0	SUB73640
	BSK1=X*ALOG(Y)*BSI1+1.0	SUB73650
	Y=Y*Y	SUB73660
	BSK1=BSK1+Y*(0.15443144+Y*(-0.67278579+Y*(-0.18156897+Y*	SUB73670
	1(-0.01919402+Y*(-0.00110404+Y*(-0.00004586))))))	SUB73680
	RESL=BSK1/X	SUB73690
	GO TO 60	SUB73700
50	Y=2.0/X	SUB73710
	BSK1=1.25331414+Y*(0.23498619+Y*(-0.03655620+Y*(0.01504268+Y*	SUB73720
	1(-0.00780353+Y*(0.00325614+Y*(-0.00068245))))))	SUB73730
	RESL=BSK1/(SORT(X)*EXP(X))	SUB73740
60	RETURN	SUB73750
	END	SUB73760
	FORTRAN NLSTOU,DECK	SUB73770
	INCODE IBMF	SUB73780
CCRN	CRNL	SUB73790
	COMPLEX FUNCTION CRNL(CX,X,Y,CK,B2)	SUB73800
	COMMON/C2/CLFN,SN,NLY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN	SUB73810
	R=ABS(Y)	SUB73820
	R2=R*R	SUB73830
	CK1=CK*R	SUB73840
	G1=0.0	SUB73850
	G3=0.0	SUB73860
	G4=0.0	SUB73870
5	S2=X*X+R2*R2	SUB73880
	S=SORT(S2)	SUB73890
	U1=(CK*S-X)/(R2*R)	SUB73900
	UK=CK1*U1	SUB73910
	DO 20 I=1,NGSKRN	SUB73920
	UZ=U1*ZKER(I)	SUB73930
	UZ2=UZ**2	SUB73940
	G=UK*ZKER(I)	SUB73950
	F=HKFR(I)/SORT(1.0+UZ2)*UZ*U1	SUB73960
	G3=G3+F*COS(G)	SUB73970
	G4=G4+F*SIN(G)	SUB73980
	V=1.0-ZKER(I)**2	SUB73990
	F=HKFR(I)*2.0*V*EXP(-CK1*V)/SORT(1.0+V)	SUB74000
20	G1=G1+F	SUB74010
	G7=G1+G3	SUB74020
	XS=X/S	SUB74030
	IF(CK.NE.0.0) GO TO 22	SUB74040
	F14=1.0	SUB74050
	GO TO 23	SUB74060
22	F14=CK1*RESL(CK1)	SUB74070
23	G1=CK1*G4-F14-XS*COS(UK)	SUB74080
	G2=CK1*G7+XS*SIN(UK)	SUB74090
	XK=CK*X	SUB74100
	CU=COS(XK)	SUB74110
	SI=SIN(XK)	SUB74120
	CRNL=CMPLX((CU*G1+SI*G2)/R2,(CO*G2-SI*G1)/R2)	SUB74130
	RETURN	SUB74140
	END	SUB74150
	FORTRAN NLSTOU,DECK	SUB74530
	INCODE IBMF	SUB74540
CCORD	CORD	SUB74550
	SUBROUTINE CORD	SUB74560
	COMPLEX A,AA,ANM,CZERO	SUB74570
	COMPLEX AK,H2,TRM,D1,CRNL	SUB74580
	COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO	SUB74590
	COMMON/C2/CLFN,SN,NLY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN	SUB74600
28	COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO	SUB74610



	COMMON/C4/MNODES,LCOLL,LPRN5H,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT	SUB74620
	COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),IL(50),HCR(6),ZCOR(6),MACH	SUB74630
	COMMON/C6/WXCHN(11),WHCH(11),WBIN(11),WT(90),XCOLL,YCOLL,P1,U	SUB74640
	COMMON/C7/CO(10,28,2),NZCO(15,2),EM,EK,B2,NWIX,NCIX,WBO,CBON,NWCY	SUB74650
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2	SUB74660
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN	SUB74670
C	THIS SUBROUTINE CONSTRUCTS A ROW OF THE DOWNWASH MATRIX	SUB74680
C	THE PRESSURE SERIES IS A PRODUCT OF CHERYSHEV POLYNOMIALS IN THE	SUB74690
C	NEGATIVE OF PERCENT SEMI-CHORD FROM THE MID-CHORD AND PERCENT	SUB74700
C	SEMI-SPAN FROM THE ROOT.	SUB74710
	DO 6 JC=1,NCOLS	SUB74720
6	A(JC) = CZERO	SUB74730
	IC1 = 0	SUB74740
	NIX = NWIX	SUB74750
	QWX = -QWXX*SN**2/(8.0*PI)	SUB74760
	NPX = NWPX	SUB74770
C	THE DO 14 LOOP COMPUTES THE NON-SINGULAR PORTION OF D(N,M)	SUB74780
C	DUE TO BOTH SURFACES	SUB74790
	DO 14 MSURF=1,2	SUB74800
	IF (MSURF.NE.NSURF.AND.ISOLAT.NE.0) GO TO 13	SUB74810
	DO 12 IY=1,NIY	SUB74820
	ETA1 = SN*ETA(IY)	SUB74830
	E12 = ETA(IY)**2	SUB74840
	IF (NPY.GT.1) CALL CHEB(NPY-1,ETA(IY),UY(2))	SUB74850
	UY(1) = 1.0 -FT2	SUB74860
	DO 3 K=2,NPY	SUB74870
3	UY(K) = E12*UY(1)*UY(K)	SUB74880
	DO 10 IX=1,NIX	SUB74890
	XI = XS(2,MSURF,IX,IY)	SUB74900
	XID = XCOLL -XI	SUB74910
	AK = CRNL(EK,XID,YCOLL-ETA1,EK,B2) + CRNL(EK,XID,YCOLL+ETA1,EK,B2)	SUB74920
	IC = IC1 +1	SUB74930
	H2 = AK*QWX*QWY	SUB74940
	IF (NPX.GT.1) CALL CHEB(NPX-1,-SIX(IX,MSURF),UX(2))	SUB74950
	UX(1) = 1.0 -SIX(IX,MSURF)	SUB74960
	DO 4 K=2,NPX	SUB74970
4	UX(K) = (1.0 +SIX(IX,MSURF))*UX(1)*UX(K)	SUB74980
C	** ADD AN INCREMENT TO EACH ELEMENT OF THE ROW FOR (XI,ETA1) **	SUB74990
	DO 10 NY=1,NPY	SUB75000
	TRM = H2 * UY(NY)	SUB75010
	DO 10 NX=1,NPX	SUB75020
	A(IC) = A(IC) +TRM*UX(NX)	SUB75030
10	IC = IC+1	SUB75040
C	** IC EQUALS NPY*NWPX+1 AT THE END OF THE FIRST PASS **	SUB75050
12	CONTINUE	SUB75060
13	NIX = NCIX	SUB75070
	QWX = -QWCX*SN**2/(8.0*PI)	SUB75080
	NPX = NCPX	SUB75090
14	IC1 = NPY*NWPX	SUB75100
	IC1 = 0	SUB75110
	NPX = NWPX	SUB75120
	XCOLS = XS(1,NSURF,ILX,I1Y)	SUB75130
	Y2 = Y(I1Y)**2	SUB75140
	CALL CHEB(NPY-1,Y(I1Y),UY(2))	SUB75150
	UY(1) = -2.0	SUB75160
	DO 15 K=2,NPY	SUB75170
15	UY(K) = -2.0*Y2*UY(K)	SUB75180
	DO 40 MSURF=1,NSURF	SUB75190
C	** THIS LOOP ADDS THE CONTRIBUTION OF THE SINGULAR INTEGRAL	SUB75200
C	ALONG THE LINE FROM THE WING L.E. TO THE COLLOCATION POINT	SUB75210
	IF (MSURF.NE.NSURF.AND.ISOLAT.NE.0) GO TO 23	SUB75220

```

IF(NSURF.LE.HSURF) GO TO 16
UPLIM = PI
GO TO 18
16 XI = SCX(IIY,NSURF)
UPLIM = -ATAN(SQRT(1.0-XT**2)/XT)
IF(UPLIM.LT.0.0) UPLIM=UPLIM+PI
18 QWSNG = FLOAT(2*NIY)*UPLIM/8.0
DO 22 N=1,6
IC = IC+1
C ** THIS LOOP CONSTRUCTS D(0,M) ,M=0,1,...,NPX-1
VINI = UPLIM*ZCOR(N)
C = COS(VINI)
CALL CHEB(NPX-1, C,UX(2))
UX(1) = 1.0 +C
DO 19 K=2,NPX
19 UX(K) = (1.0 -C)*UX(1)+UX(K)
ARG = EK*(XCOLS -WXCHN(IIY) +C*WBCN(IIY))
IF(HSURF.EQ.2) ARG=EK*(XCOLS-CXMN+C*CBON)
C1 = COS(ARG)
S1 = SQRT(1.0 -C1**2)
D1 = CMPLX(C1,-S1)*HCOR(N)
DO 22 NY=1,NPY
TRM = QWSNG*UY(NY)*D1
DO 22 NX=1,NPX
A(IC) = A(IC) +TRM*UX(NX)
22 IC = IC+1
23 ICI = NPY*NWPX
40 NPX = NCPX
RETURN
END
$ FORTRAN NLIST00,DECK
$ INCODE IBMF
CZDZX ZDZX
SUBROUTINE ZDZX(MODE,DZ,Z)
COMPLEX A,AA,ANM,CZERO
COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRN
COMMON/C3/NPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),IIY,IIY,NSURF,ISOLAT
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),II(50),HCOR(6),ZCOR(6),MACH
COMMON/C6/WXCHN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U
COMMON/C7/CU(10,28,2),NZCO(10,2),EK,EK,2,NWIX,NCIX,WBO,CBON,NWCY
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXTMN(11),E1,E2
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWHX,QWCX,CXHN
PX = XCOLL * WBO
IF(NSURF.GT.1) PX=PX-CLEN*WBO
PY = YCOLL * WBO
Z= CO(MODE,1,NSURF)
DZ = 0.0
K = 2
YX = PY/PX
PPX = PX
DO 40 N = 2,7
PXY = PPX
F = N-1
DO 30 M = 1,N
IF(K.GT.NZCO(MODE,NSURF)) GO TO 50
ZP = PXY * CO(MODE,K,NSURF)
Z = Z + ZP
DZ = DZ + ZP * F

```

SUB75230  
SUB75240  
SUB75250  
SUB75260  
SUB75270  
SUB75280  
SUB75290  
SUB75300  
SUB75310  
SUB75320  
SUB75330  
SUB75340  
SUB75350  
SUB75360  
SUB75370  
SUB75380  
SUB75390  
SUB75395  
SUB75400  
SUB75410  
SUB75420  
SUB75430  
SUB75440  
SUB75450  
SUB75460  
SUB75470  
SUB75480  
SUB75490  
SUB75500  
SUB75510  
SUB74160  
SUB74170  
SUB74180  
SUB74190  
SUB74200  
SUB74210  
SUB74220  
SUB74230  
SUB74240  
SUB74250  
SUB74260  
SUB74270  
SUB74280  
SUB74290  
SUB74300  
SUB74310  
SUB74320  
SUB74330  
SUB74340  
SUB74350  
SUB74360  
SUB74370  
SUB74380  
SUB74390  
SUB74400  
SUB74410  
SUB74420  
SUB74430  
SUB74440  
SUB74450

```

    PXY = PXY*YX
    F = F - 1.0
30 K = K + 1
40 PPX = PPX + PX
50 DZ = DZ/PX
    RETURN
    END

```

```

$   FORTRAN NLSTOU,DECK
$   INCODE IBMF
CCGRFD   CGRED

```

```

SUBROUTINE CGRED(V,IR,IC)
COMPLEX ANM,CZERO
DIMENSION V(2,1)
COMMON/C1/A(2,60),AA(2,50,60),ANM(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUB
COMMON/C3/HPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIUNCX,RHO SUB
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT SUB
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),I1(50),HCUR(6),ZCUR(6),MACH SUB
COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U SUB
COMMON/C7/CU(10,28,2),NZCO(10,2),EM,EK,12,NWIX,NCIX,WBO,CBON,NWCY SUB
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2 SUB
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN SUB
RMN = SQRT(AA(1,IR,IC)**2 + AA(2,IR,IC)**2) SUB
IF(AA(2,IR,IC).LE.E2) GO TO 30 SUB
CR = AA(1,IR,IC)/RMN SUB
CI = AA(2,IR,IC)/RMN SUB
DO 20 N=IC,MAUG SUB
TI = CR*AA(1,IR,N) + CI*AA(2,IR,N) SUB
AA(2,IR,N) = CR*AA(2,IR,N) - CI*AA(1,IR,N) SUB
20 AA(1,IR,N) = TI SUB
30 RAN = SQRT(V(1,IC)**2 + V(2,IC)**2) SUB
IF(RAN.LE.E2) GO TO 60 SUB
RAN = SQRT(RAN**2 + RMN**2) SUB
CR = V(1,IC)/RAN SUB
CI = V(2,IC)/RAN SUB
RMN = RMN/RAN SUB
DO 50 N=IC,MAUG SUB
AIR = RMN*AA(1,IR,N) + CR*V(1,N) + CI*V(2,N) SUB
AII = RMN*AA(2,IR,N) + CR*V(2,N) - CI*V(1,N) SUB
VR = RMN*V(1,N) - CR*AA(1,IR,N) + CI*AA(2,IR,N) SUB
VI = RMN*V(2,N) - CR*AA(2,IR,N) - CI*AA(1,IR,N) SUB
AA(1,IR,N) = AIR SUB
AA(2,IR,N) = AII SUB
V(1,N) = VR SUB
50 V(2,N) = VI SUB
60 RETURN
    END

```

```

$   FORTRAN NLSTOU,DECK
$   INCODE IBMF
CXLSO   XLSO

```

```

SUBROUTINE XLSO
COMPLEX A,AA,ANM,CZERO
COMMON/C1/A(60),AA(50,60),ANM(50,10),CZERO
COMMON/C2/CLEN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUB
COMMON/C3/HPY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIUNCX,RHO SUB
COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT SUB
COMMON/C5/FW,FC,NCOLS,NOMIT,ALPHA(10),I1(50),HCUR(6),ZCUR(6),MACH SUB
COMMON/C6/WXCMN(11),WBCN(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U SUB
COMMON/C7/CU(10,28,2),NZCO(10,2),EM,EK,12,NWIX,NCIX,WBO,CBON,NWCY SUB
COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIMN(11),E1,E2 SUB
COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN SUB

```

SUB74460  
 SUB74470  
 SUB74480  
 SUB74490  
 SUB74500  
 SUB74510  
 SUB74520  
 SUB75520  
 SUB75530  
 SUB75540  
 SUB75550  
 SUB75560  
 SUB75570  
 SUB75580  
 SUB75590  
 SUB75600  
 SUB75610  
 SUB75620  
 SUB75630  
 SUB75640  
 SUB75650  
 SUB75660  
 SUB75670  
 SUB75680  
 SUB75690  
 SUB75700  
 SUB75710  
 SUB75720  
 SUB75730  
 SUB75740  
 SUB75750  
 SUB75760  
 SUB75770  
 SUB75780  
 SUB75790  
 SUB75800  
 SUB75810  
 SUB75820  
 SUB75830  
 SUB75840  
 SUB75850  
 SUB75860  
 SUB75870  
 SUB75880  
 SUB75890  
 SUB75900  
 SUB75910  
 SUB75920  
 SUB75930  
 SUB75940  
 SUB75950  
 SUB75960  
 SUB75970  
 SUB75980  
 SUB75990  
 SUB76000  
 SUB76010  
 SUB76020  
 SUB76030  
 SUB76040  
 SUB76050

```

      I1 = 1
      DO 136 I=1,NCOLS
      RII = CABS(AA(I1,I))
      IF(RII.LE.E2) GO TO 135
      IL(I) = I1
      I1 = I1 + 1
      GO TO 136
135  IL(I) = -1
      I12 = NCOLS - 1 - (I-I1)
      DO 1135 I1=I1,I12
1135  CALL CGRED(AA(I1+1,I),I1,I+1)
      DO 2135 L=1,NMODES
      ML = NCOLS + L
2135  ALPHA(L) = SORT(ALPHA(L)**2 + CABS(AA(I12+1,ML))**2)
136  CONTINUE
C      SOLVE FOR THE COEFFICIENTS BY BACK SUBSTITUTION
140  I1 = NCOLS
      DO 150 I = 1,NCOLS
      DO 150 L=1,NMODES
150  ANH(I,L) = CZERO
      DO 210 J=1,NCOLS
      IF(IL(I1).LE.0) GO TO 210
      J1 = IL(I1)
      DO 200 L=1,NMODES
      ML = NCOLS + L
      IF(I1-NCOLS) 170,190,220
170  IK = I1 + 1
      DO 180 K=IK,NCOLS
180  ANH(I1,L) = ANH(I1,L) - AA(J1,K)*ANH(K,L)
190  ANH(I1,L) = (ANH(I1,L) + AA(J1,ML))/AA(J1,I1)
200  CONTINUE
210  I1 = I1 - 1
220  RETURN
      END
S      FORTRAN NLSTOU,DECK
S      INCODE IBMF
CCHER      CHEB
      SUBROUTINE CHEB(N1,X,UX)
      DIMENSION UX(1)
      DO 10 I=1,N1
10  UX(I) = 0.0
      UX(1) = 1.0
      UX(2) = 2.0*X
      IF(N1.LT.3) RETURN
      DO 20 I=3,N1
20  UX(I) = 2.0*X*UX(I-1) - UX(I-2)
      RETURN
      END
S      FORTRAN NLSTOU,DECK
S      INCODE IBMF
CFORC      FORC
      SUBROUTINE FORC(NWICX,NCICX,NICY,YEIA,SICX,WBICN,LPR)
      COMPLEX A,AA,ANH,CZERO,GFORC,DELP,WASH,APR,DWASH,CWASH,PR
      DIMENSION YITA(1),SICX(1),WBICN(1)
      DIMENSION DWASH(90,10),PR(90,10),CWASH(40,10)
      DIMENSION GFORC(10,10,3),DELP(10),WASH(10)
      COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO
      COMMON/C2/CLFN,SN,NFY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUR
      COMMON/C3/NFY,SOUND,NMACH,FMACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO
      COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NOM(5),I1Y,I1X,NSURF,ISOLAT

```

SUB76060  
 SUB76070  
 SUB76080  
 SUB76090  
 SUB76100  
 SUB76110  
 SUB76120  
 SUB76130  
 SUB76140  
 SUB76150  
 SUB76160  
 SUB76170  
 SUB76180  
 SUB76190  
 SUB76200  
 SUB76210  
 SUB76220  
 SUB76230  
 SUB76240  
 SUB76250  
 SUB76260  
 SUB76270  
 SUB76280  
 SUB76290  
 SUB76300  
 SUB76310  
 SUB76320  
 SUB76330  
 SUB76340  
 SUB76350  
 SUB76360  
 SUB76370  
 SUB76380  
 SUB76390  
 SUB76400  
 SUB76410  
 SUB76420  
 SUB76430  
 SUB76440  
 SUB76450  
 SUB76460  
 SUB76470  
 SUB76480  
 SUB76490  
 SUB76500  
 SUB76510  
 SUB76520  
 SUB76530  
 SUB76540  
 SUB76550  
 SUB76560  
 SUB76570  
 SUB76580  
 SUB76590  
 SUB76600  
 SUB70370  
 SUB76620  
 SUB76630  
 SUB76640  
 SUB76650

	COMMON/C5/FW,FC,NCOLS,NONIT,ALPHA(10),IL(58),HCOR(6),ZCOR(6),MACH	SUB76660
	COMMON/C6/WXCHN(11),WBCN(11),WBCN(11),WT(90),XCOLL,YCOLL,PI,U	SUB76670
	COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,H2,NHIX,NCIX,WBO,CBON,NWCY	SUB76680
	COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIHN(11),E1,E2	SUB76690
	COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWXX,QWCX,CXMN	SUB76700
	COMMON/CPR/APR(90,60),IMOD,IROW	SUB76710
	EQUIVALENCE (GFORC,AA),(A,WASH),(WASH,DEL P)	SUB76720
	EQUIVALENCE (WASH(1,1),APR(1,51)),(PR(1,1),APR(1,11))	SUB76730
	EQUIVALENCE (WASH(1,1),APR(1,41))	SUB76740
	QWF = 0.5*RHO*(U*WBO*SN)**2 *QWY	SUB76750
	IF(LPR.NE.0) GO TO 2	SUB76760
	DO 1 I=1,NMODES	SUB76770
	DO 1 J=1,NMODES	SUB76780
	DO 1 K=1,2	SUB76790
	1 GFORC(I,J,K) = CZERO	SUB76800
	2 IC1 = 0	SUB76810
	NICX = NWICX	SUB76820
	NPX = NWPX	SUB76830
	QWFORC = QWF*QWXX	SUB76840
	IROW = 1	SUB76850
	LMNT1 = 40	SUB76860
	IF(LPR.NE.0) LMNT1 = 10	SUB76870
	DO 1000 NS=1,2	SUB76880
	NSURF = NS	SUB76890
	PFAC = SN/CBON	SUB76900
	DO 900 I1Y=1,NICY	SUB76910
	YCOLL = Y-ETA(I1Y)	SUB76920
C	** YCOLL, AND LATER XCOLL, ARE USED HERE TO DENOTE INTEGRATION	SUB76930
C	STATIONS BECAUSE WE USE SUBROUTINE ZOX TO COMPUTE THE	SUB76940
C	DISPLACEMENT THROUGH WHICH THE PRESSURE ACTS TO DO WORK	SUB76950
	Y2 = YCOLL**2	SUB76960
	IF(NPY.GT.1) CALL CHER(NPY-1,YCOLL,UY(2))	SUB76970
	UY(1) = 1.0 -Y2	SUB76980
	IF(LPR.NE.0) UY(1)=SQRT(1.0-Y2)	SUB76990
	DO 3 K=2,NPY	SUB77000
	3 UY(K) = Y2*UY(1)*UY(K)	SUB77010
	IF(NSURF.EQ.1) PFAC=SN/WBCN(I1Y)	SUB77020
	YCOLL = SN*YCOLL	SUB77025
	DO 800 I1X=1,NICX	SUB77030
	LMNT1 = I1X +LMNT1*(NSURF-1)	SUB77040
	XCOLL = SIX(LMNT1)	SUB77050
	IF(NPX.GT.1) CALL CHER(NPX-1,-XCOLL,UX(2))	SUB77060
	UX(1) = 1.0 -XCOLL	SUB77070
	IF(LPR.NE.0) UX(1)=SQRT(UX(1)/(1.0+XCOLL))	SUB77080
	DO 4 K=2,NPX	SUB77090
	4 UX(K) = (1.0 +XCOLL)*UX(1)*UX(K)	SUB77100
	IC = IC1 +1	SUB77110
	DO 10 J=1,NMODES	SUB77120
	10 DELP(J) = CZERO	SUB77130
	DO 200 NY=1,NPY	SUB77140
	DO 200 NX=1,NPX	SUB77150
	DO 20 J=1,NMODES	SUB77160
	DELP(J) = DELP(J) +UX(NX)*UY(NY)*ANM(IC,J)	SUB77170
	IF(LPR.NE.0) PR(IROW,J) = DELP(J)*PFAC	SUB77180
	20 CONTINUE	SUB77190
	200 IC = IC+1	SUB77200
C	** IC = NPY*NWPX+1 AT THE END OF THE NS=1 PASS	SUB77210
C	AND DP CONTAINS DELTA P/Q AT (XCOLL,YCOLL)	SUB77220
	IROW = IROW + 1	SUB77230
	IF(LPR.NE.0) GO TO 800	SUB77240
	XCOLL = XS(2,NS,I1X,I1Y)	SUB77245

```

DO 400 I=1,NMODES
  CALL ZDZX(1,SLOPE,DISP)
  DO 400 J=1,NMODES
400  GFORC(1,J,NS) = GFORC(1,J,NS) + QWFORC*DISP*DELP(J)*2.0
800    CONTINUE
900    CONTINUE
      NICX = NCICX
      NPX = NCPX
      IC1 = IC-1
      QWFORC = QW1 + QWCX
1000  CONTINUE
      RETURN
      END
S      FORTRAN NLSTOD,DECK
S      INCODE IBMF
CKOUT  KOUT
SUBROUTINE KOUT(IND)
  COMPLEX A,AA,ANH,CZERO,GFORC,DELP,WASH,APR,DWASH,CWASH,PR
  DIMENSION CARDS(25,50)
  DIMENSION GFORC(10,10,3),DELP(10),WASH(10)
  DIMENSION DWASH(90,10),PR(90,10),CWASH(90,10)
  DIMENSION SURF(2,3),XPR(50)
  COMMON/C1/A(60),AA(50,60),ANH(50,10),CZERO
  COMMON/C2/CLFN,SN,NIY,NWCX,NCCX,NWPX,NCPX,HKER(20),ZKER(20),NGSKRNSUR77250
  COMMON/C3/NPY,SOUND,NHACH,FHACH(6),NFREQ,FREQ(10),MAUG,NIONCX,RHO SUR77260
  COMMON/C4/NMODES,LCOLL,LPRWSH,LPRCO,NUM(5),I1Y,I1X,NSURF,ISOLAT SUR77270
  COMMON/C5/FW,FC,NCOLS,HOMIT,ALPHA(10),IL(50),HCOR(6),ZCOR(6),HACH SUR77280
  COMMON/C6/WXCHN(11),WACH(11),WBIN(11),WI(90),XCOLL,YCOLL,PI,U SUR77290
  COMMON/C7/CO(10,28,2),NZCO(10,2),EM,EK,K2,NWIX,NCIX,WBO,CBON,NWCY SUR77300
  COMMON/C8/IFR,XE(5),YE(3),UX(10),UY(10),WXIHN(11),E1,E2 SUR77310
  COMMON/C9/SIX(40,2),SCX(10,2),Y(11),ETA(11),QWY,QWWX,QWCX,CXHN SUR77320
  COMMON/CPR/APP(90,60),IMOD,IRON SUR77330
  EQUIVALENCE (GFORC,AA),(A,WASH),(WASH,DELP) SUR77340
  EQUIVALENCE (DWASH(1,1),APR(1,51)),(PR(1,1),APR(1,11)) SUR77350
  EQUIVALENCE (CWASH(1,1),APR(1,41)) SUR77360
  EQUIVALENCE (XPR,IL) SUR77370
  DATA (SURF(1,1),I=1,3)/6HWING ,RHTAIL ,11HWING + IAIL / SUR77380
  GO TO (10,20,30,40,50,60,70,80,90),IND SUR77390
C ***** SUR77400
10  XY = XE(5) - XF(4) SUR77410
  XX = XE(3) - XF(2) SUR77420
  AY = 2.0*XE(3)*YE(3) - XE(2)*(YE(3)-YE(2)) SUR77430
  AX = 2.0*XV*YE(3) SUR77440
  WRITE(6,11)EM,SOUND,RHO,XE(1),XE(4),XE(3),XV,YE(2),YE(3),YE(3), SUR77450
  1YE(3),XX,XV,AW,AT,NWCY,NIY,NWCX,NCCX,NWIX,NCIX,NPY,NPY,NWPX,NCPX SUR77460
11  FORMAT(1H1//// 31X,41HACH/NAA MISSILE SUBSONIC AIRLOADS PROGRAM SUR77470
  1 ///37X,30HHEIGHT CONDITIONS AND GEOMETRY/1H0//15X, 13HMACH NUMBER SUR77480
  2 =,18.5,4X,16HSPEED OF SOUND =F10.3,4H L/T,4X,4HRHO=,E14.8//1H0/ SUR77490
  X54X,4HWING,18X, SUR77500
  3 4HTAIL///22X,16HLE. STATION (L),2F22.3//22X,16HROOT CHORD. (L), SUR77510
  4 2F22.3// 22X,16HLE. SPAN (L),2F22.3//22X,16HT.E. SPAN (L), SUR77520
  5 2F22.3// 22X,16HTIP CHORD (L),2F22.3//22X,16HTOTAL AREA (L*L) SUR77530
  6 2F22.3//22X,16HSPAN COLL. STA.,119,122,//22X,16HCHORD COLL. STA. SUR77540
  7 119,122//22X,16HCHORD INIG. STA.,119,122//22X,16HSPAN PRES MODES SUR77550
  8,119,122//22X,16HCHORD PRES MODES,119,122) SUR77560
  IF(MACH(MACH).LE.0.95) GO TO 15 SUR77570
  WRITE(6,14) SUR77580
  14 FORMAT(92H A MACH NUMBER GREATER THAN 0.95 HAS BEEN USED----- SUR77590
  10USE CAUTION IN APPLYING CASE RESULTS) SUR77600
  15 IF(NOMIT.EQ.0) RETURN SUR77610

```

```

WRITE(6,12)(NOH(I),I=1,NOH1)
12 FORMAT(1H0,15X,51H THE SPANWISE COLLOCATION STATION(S) OMITTED ON HSUB77850
1ING,915)
RETURN
C *****
20 NCX = NWCX
NIX = NWIX
DO 150 NS=1,2
WRITE(6,22)(SURF(1,NS),I=1,2)
22 FORMAT(1H1,31X,42H MISSILE SUBSONIC AIRLOADS PROGRAM (CONT-D)/1H / SUB77930
1 25X,39H COLLOCATION STATION COORDINATES ON THE 2A6/1H0,12H S STSUB77940
2A NO,7X,2HYC,8X,7X,11HXC VALUES--)
DO 123 IY=1,NIY
YC = WBO*SN*Y(IY)
DO 120 IX=1,NCX
120 XPR(IX) = WBO*XS(1,NS,IX,IY)
123 WRITE(6,124) IY,YC,(XPR(IX),IX=1,NCX)
124 FORMAT(1H0,112,5E17.6/(1H ,29X,4E17.6))
WRITE(6,105) (SURF(1,NS),I=1,2)
105 FORMAT(1H0,24X,39H INTEGRATION STATION COORDINATES ON THE 2A6/1H0,
112H S STA NO,7X,2HYI,8X,7X,11HXI VALUES--)
DO 106 IY=1,NIY
YI = WBO*SN*FTI(IY)
DO 126 IX=1,NIX
126 XPR(IX) = WBO*XS(2,NS,IX,IY)
106 WRITE(6,124) IY,YI,(XPR(IX),IX=1,NIX)
NCX = NCCX
NIX = NCIX
150 CONTINUE
RETURN
C *****
30 DO 34 NS = 1,2
WRITE(6,21) IREQ(IFR),NMODES,EK,EH
21 FORMAT(1H1,31X,42H MISSILE SUBSONIC AIRLOADS PROGRAM (CONT-D)//1H /SUB/8170
1 9X,27H OSCILLATORY FREQUENCY (CPS),F12.5,13X,12,17H DEFLECTION MODSUB8180
2ES/1H0,8X,30H REDUCED FREQUENCY (SEMI CHORD),F9.5,14X,23H FREE STREASUB8190
3M MACH NUMBER,F9.3/1H )
WRITE(6,31) IMOD
31 FORMAT(34X,34H PRESSURE COEFFICIENTS FOR MODE NO.13//19X,1H11X,10HSUB8220
1R COEFF(1)12X,10H1 COEFF(1) 9X,9H SPAN MODE 3X,10H CHORD MODE,)
WRITE(6,32)(SURF(KI,NS),KI=1,2)
32 FORMAT(1H0,9X,2A6//)
GO TO(2,3),NS
2 NL = NWPX
ML = NPY
IK = 1
GO TO 4.
3 NL = NCPX
ML = NPY
IK = NWPX*NPY+1
4 DO 6 IM = 1,ML
DO 6 IN = 1,NL
WRITE(6,33) IK,ANN(IK,IMOD),IM,IN
33 FORMAT(1H0,119,1P2E22.5,2113)
6 IK = IK + 1
34 CONTINUE
RETURN
C *****
40 WRITE(6,41)
41 FORMAT(1H0,20X,38H ERROR IN INPUT DATA (NO TAIL) REQUIRES//,21X,19HSUB8430
1TERMINATION OF CASE)

```

```

CALL EXIT SUB78450
C ***** SUB78460
50 WRITE(6,51) SUB78470
51 FORMAT(1H0,20X,63HNUMBER OF COLLOCATION OR INTEGRATION STATIONS OR SUB78480
1 PRESSURE TERMS//21X,25HEXCEEDS ALLOWABLE MAXIMUM//35X,18HCASE ISSUB78490
2 TERMINATED) SUB78500
CALL EXIT SUB78510
C ***** SUB78520
60 WRITE(6,21)FRQ(IFR),NMODES,EK,EM SUB78530
WRITE(6,101) SURF(1,NSURF) SUB78540
101 FORMAT(1H0,27X,45HINPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR ,A6SUB78550
1//22X,62HREFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSESUB78560
2CTION //2X,4HMODE,20X, 7HCOEFFS.) SUB78570
DO 69 L=1,NMODES SUB78580
NTM = NZCO(L,NSURF) SUB78590
WRITE(6,66) L,(CO(L,K,NSURF),K=1,NTM) SUB78600
66 FORMAT(1H0,14,4X,1P7E13.4/(9X,1P7E13.4)) SUB78610
69 CONTINUE SUB78620
RETURN SUB78630
C ***** SUB78640
70 WRITE(6,21)FRQ(IFR),NMODES,EK,EM SUB78650
WRITE(6,35) ALPHA(IMOD) SUB78660
35 FORMAT(24X,47H RMS ERROR OF DOWNWASHES AT COLLOCATION POINTS =,1E13SUB78670
X.6) SUB78680
WRITE(6,36) IMOD SUB78690
36 FORMAT(1H0,23X,57HPRESSURES AND UPWASHES AT COLLOCATION POINTS FORSUB78700
X MODE NO.13) SUB78710
WRITE(6,32)(SURF(L,NSURF),L=1,2) SUB78720
WRITE(6,37) SUB78730
37 FORMAT(1H0,7X,1HX,8X,1HY,9X,8HR P(X,Y),5X,8HI P(X,Y),6X, SUB78740
1 9HR CW(X,Y),4X,9HI CW(X,Y),6X,9HR DW(X,Y),4X,9HI DW(X,Y)) SUB78750
RETURN SUB78760
C ***** SUB78770
80 WRITE(6,21)FRQ(IFR),NMODES,EK,EM SUB78780
WRITE(6,61) (SURF(L,NSURF),L=1,2) SUB78790
61 FORMAT(35X,23HGENERALIZED FORCES FOR 2A//1H0,6X,4HDEFL,3X,4HLOAD,1SUB78800
10X,9HREAL PART,10X,9HIMAG PART,10X,9HABS. VALUE,10X,11HPHASE ANGLE/SUB78810
2/) SUB78820
DO 78 I=1,NMODES SUB78830
DO 78 J=1,NMODES SUB78840
IF(NSURF.EQ.3) GO TO 76 SUB78850
G1 = REAL(GFORC(I,J,NSURF)) SUB78860
G2 = AIMAG(GFORC(I,J,NSURF)) SUB78870
GO TO 77 SUB78880
76 G1 = REAL(GFORC(I,J,1)) + REAL(GFORC(I,J,2)) SUB78890
G2 = AIMAG(GFORC(I,J,1)) + AIMAG(GFORC(I,J,2)) SUB78900
KKK=2*NMODES *****
NNN=2*J-1 *****
NNNN=2*J *****
CARDS(I,NNN)=G1 *****
CARDS(I,NNNN)=G2 *****
/7 G3 = SQRT(G1**2+G2**2) SUB78910
G4 = 0.0 SUB78920
IF(G3.NE.0.0) G4 = 57.2957795*ATAN2(G2,G1) SUB78930
WRITE(6,71) I,J,G1,G2,G3,G4 SUB78940
IF(NSURF.NE.3) GO TO 78 *****
IF(I.NE.NMODES) GO TO 78 *****
IF(J.NE.NMODES) GO TO 78 *****
PUNCH 6969, ((CARDS(I,JJ),JJ=1,KKK), I=1,NMODES) *****
6969 FORMAT(1P6F12.5)
71 FORMAT(1H0,19,17.2X,1P3E19.5,0PF16.3,4H DEG)

```



78 CONTINUE  
RETURN

SUB78960  
SUB78970

C

\*\*\*\*\*  
90 WRITE(6,19) XCOLL,YCOLL,PR(IROW,IMOD),C=ASH(IROW,IMOD),  
X DWASH(IROW,IMOD)

SUB78980  
SUB78990  
SUB79000

19 FORMAT(1H0,2X,2F9.3,2X,2E13.4,2X,2E13.4,2X,2E13.4)  
RETURN  
END

SUB79010  
SUB79020  
SUB79030

## 4.0 TRANSONIC UNSTEADY AERODYNAMICS PROGRAM

### 4.1 Theoretical Derivation

When the flight speed approaches  $M = 1.0$ , the velocity potential equation can be written as

$$\phi_{yy} + \phi_{zz} = M^2 (2ik\phi_x - k^2\phi) \quad (4.1.1)$$

which is valid if  $k \gg |M-1|$ . The linearized equation is applicable when the lifting surfaces are oscillating rapidly such that non-linear disturbances in the flow do not have time to accumulate.

Equation (4.1.1) is satisfied by a pulsating doublet which produces a velocity potential at  $(x,y,z)$  given by

$$\phi_D = \frac{1}{2} \frac{k(z-\zeta)}{(x-\xi)^2} \exp \left\{ -1/2 ik \left[ (x-\xi) + \frac{(y-\eta)^2 + (z-\zeta)^2}{(x-\xi)} \right] \right\} \quad (4.1.2)$$

where the doublet is positioned at  $(\xi, \eta, \zeta)$ . The doublet has no influence at points upstream of the line  $x = \xi$  and, consequently, the potential is zero in that region.

A solution to equation (4.1.1) may be obtained by superposition. This solution will be represented in the form

$$\phi(x,y,z) = \iint \phi(\xi, \eta) \phi_D(x,y,z,\xi,\eta,0) d\xi d\eta \quad (4.1.3)$$

where  $\phi(\xi, \eta)$  is the doublet strength of point  $(\xi, \eta)$ .

To compute the velocity potential distribution, the wing, wake and control surface is divided into a lattice of square boxes as shown in Figure 4.1.1. The potential function is replaced by a set of point values at the box centers. The potential function and downwash value is assumed constant over each box and equal to the central value.

The problem reduces to imposing boundary conditions and determining the doublet strength for each box to satisfy the boundary conditions. The boundary value problem becomes

#### 1. Tangential Flow Condition

$$w(x,y)_{\text{wing}} = \iint_{\text{wing}} \phi(\xi, \eta) \lim_{z \rightarrow 0} \frac{\partial \phi_D}{\partial z} d\xi d\eta \quad (4.1.4)$$

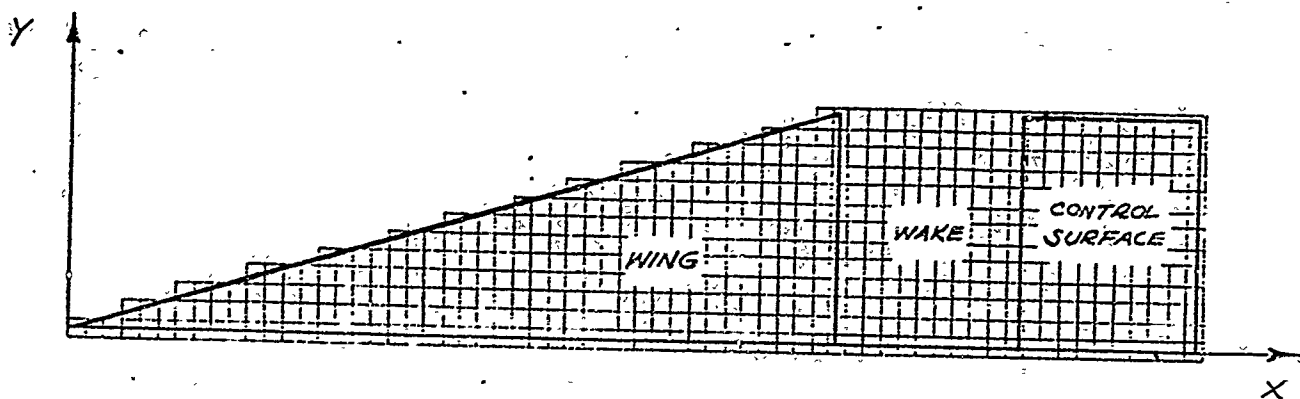


Figure 4.1.1 Sonic Box Overlay Pattern

$$w(x,y)_{\text{control surface}} = \iint_{\text{wing + wake + control surface}} \phi(\xi, \eta) \lim_{z \rightarrow 0} \frac{\partial \phi}{\partial z} d\xi d\eta \quad (4.1.5)$$

## 2. Zero Pressure Jump in Wake

$$\frac{\partial \phi}{\partial x} - ik\phi = 0 \quad (4.1.6)$$

Equation (4.1.6) is an ordinary homogeneous differential equation subjected to the condition  $\phi$  is equal to the value of the velocity potential at the wing trailing edge for  $x = x_{\text{wing t.e.}}$ . This gives the solution

$$\phi_{\text{wake}} = \phi_{\text{wing t.e.}} e^{-ik(x-x_{\text{wing t.e.}})} \quad (4.1.7)$$

Equations (4.1.4), and (4.1.5) and (4.1.7) form a system of equations from which the point values of the potential functions can be found at the box centers. The pressure distribution is then determined from the relationship

$$\Delta P(x,y) = -\frac{1}{2} \rho U^2 (2 \frac{\partial \phi}{\partial x} + 2ik\phi) \quad (4.1.8)$$

and the generalized forces are found from equation (2.0.1).

## 4.2 PROGRAM DESCRIPTION

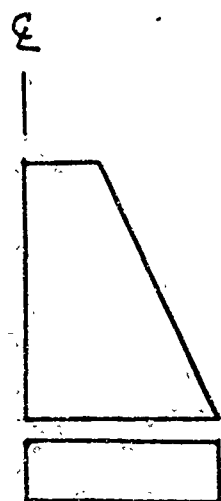
The Sonic Unsteady Aerodynamics Program calculates generalized forces for up to 10 deformation modes. The computer solution is based upon the Mach box technique. The various configurations which can be analyzed are shown in Figure 4.2.1 and Table 4.2.2. The analysis includes interaction effects between tandem surfaces and wake effects on the trailing surface. Single surfaces may be analyzed by inputting a second surface with a zero chord length.

The transonic box method calculates the unsteady potentials from which the pressure distributions may be obtained for arbitrary modes of surface motion. The method used was suggested by the successes of the supersonic box methods of Pines and others, Reference 11. The potential is generated by a doublet distribution rather than by a source distribution because the latter method would involve diaphragm regions of infinite extent, whereas the doublet distribution is confined to the wing and its wake. As with the subsonic problem, the differential equation solution is an integral equation. The integral equation is approximated numerically by a matrix equation so that the basic step in the box method is the solution of the system of simultaneous equations which determine a set of values of potential on the surface from a corresponding array of upwash values. The solution procedure obtains the velocity potential over the surface one spanwise row of boxes at a time until the trailing edge row is completed. The numerical complexity is not increased, however, by a large number of box rows over the configuration because the influence coming from more than 15 rows away has been found to be negligible. The results are valid for high reduced frequency,  $k$ , such that  $k \gg M - 1$  where  $M$  is the Mach number.

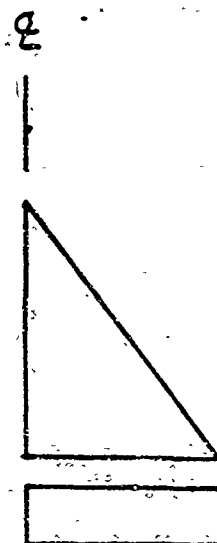
The solution for the generalized aerodynamic forces requires the input of the deformation modes due to vibration. The program considers the modes to be expressed as analytic functions of the form:

$$w(x, y) = \sum_{m=0}^N \sum_{n=0}^n C_{(n-m), m} x^{(n-m)} y^m$$

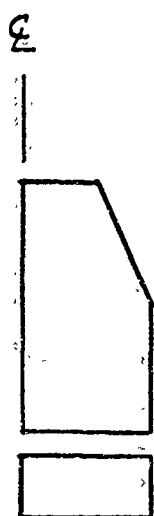
To meet this requirement only the coefficients "c" are required as input into the program. These coefficients can be obtained in several ways, the most common way is to surface fit the modes by the least-square technique.



TRAPEZOIDAL



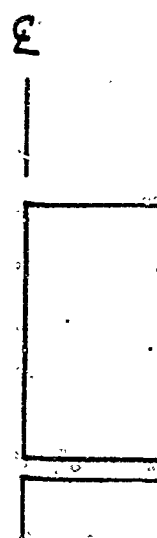
DELTA



TRAPEZOIDAL  
(CROPPED)



DELTA  
(CROPPED)



RECTANGULAR

FIGURE 4.2.1  
TANDEM COPLANAR CONFIGURATIONS AT SONIC  
MACH NUMBER

TABLE 4.2.2 OPTIONAL CONFIGURATIONS

CONFIGURATION	CHORDWISE COORDINATE	SPANWISE COORDINATE
RECTANGULAR	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) = 0.0$	$Y(2) = 0.0$
	$X(3) > 0.0$	$Y(3) > 0.0$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
DELTA	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > 0.0$	$Y(2) = 0.0$
	$X(3) = X(2)$	$Y(3) > 0.0$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
TRAPEZOIDAL	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > 0.0$	$Y(2) > 0.0$
	$X(3) = X(2)$	$Y(3) > Y(2)$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
TRAPEZOIDAL (CROPPED)	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > X(1)$	$Y(2) > 0.0$
	$X(3) > X(2)$	$Y(3) > Y(2)$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	
DELTA (CROPPED)	$X(1) = 0.0$	$Y(1) = 0.0$
	$X(2) > 0.0$	$Y(2) = 0.0$
	$X(3) > X(2)$	$Y(3) > Y(2)$
	$X(4) \geq X(3)$	
	$X(5) \geq X(4)$	

### 4.3 INPUT INSTRUCTIONS

Instructions for preparing input data for the transonic computer program are presented here. The field location and format for each quantity is specified. Any set of units may be used for geometric dimensions and acoustic velocity as long as they are consistent, e.g., if inches is used for length, then the acoustic velocity must have dimensions of inches per second. The required data and the sequence in which the information is entered is as follows:

#### 1. Streamwise Coordinates (6El2.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	X(1)	X(2)	X(3)	X(4)	X(5)	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) X(1) Wing root leading edge coordinate (See Figure 4.3.1)
- (2) X(2) Wing tip leading edge coordinate
- (3) X(3) Wing trailing edge coordinate
- (4) X(4) Control surface leading edge coordinate
- (5) X(5) Control surface trailing edge coordinate

A single surface, the wing, may be analyzed by setting X(4) and X(5) equal to X(3). The various configurations are generated as shown in Table 4.2.1. The origin for the planform and AIC station coordinates must be at the leading edge root of the wing, therefore X(1) and Y(1), described below, must always be zero.

#### 2. Spanwise Coordinates and Acoustic Velocity (6El2.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	Y(1)	Y(2)	Y(3)	SOUND	RHO	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) Y(1) Wing root spanwise coordinate
- (2) Y(2) Wing leading edge spanwise coordinate
- (3) Y(3) Wing (and control surface) tip spanwise coordinate
- (4) SOUND Speed of sound at altitude for which analysis is performed
- (5) RHO density of fluid \* 1000.0 (M./L<sup>3</sup>)



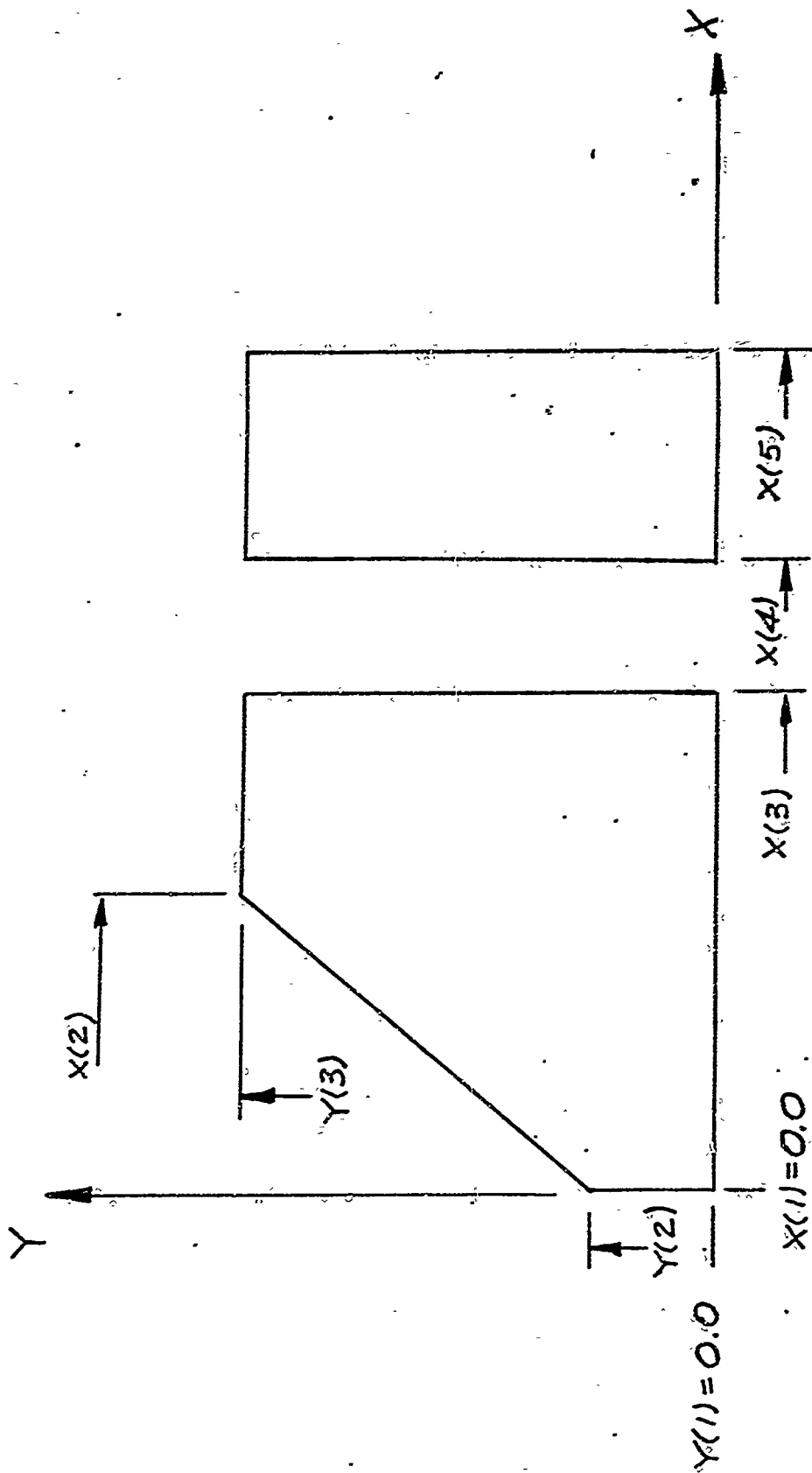


FIGURE 4.3.1  
GEOMETRY DESCRIPTION

### 3. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NMACH	NFREQ	NMODES	NBW	LVPICT	LSSVP
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NMACH Number of Mach numbers (max 6)  
 (2) NFREQ Number of input frequencies (max 10)  
 (3) NMODES Number of input modes (max 10)  
 (4) NBW Number of chordwise wing boxes (max 10)  
 (5) LVPICT Print velocity potential influence coefficients; 0 ~ No, 1 ~ Yes  
 (6) LSSVP Print upwashes; 0 ~ No, 1 ~ Yes

### 4. Mach Numbers (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FMACH(1)	FMACH(2)	FMACH(3)	FMACH(4)	FMACH(5)	FMACH(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FMACH(i) Mach numbers for which the analysis is to be performed.

### 5. Frequency (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FREQ(1)	FREQ(2)	FREQ(3)	FREQ(4)	FREQ(5)	FREQ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FREQ Frequencies for which the analysis is to be performed.  
 Continue on next card for FREQ(i) 6.

### 6. Deformation Modes. Repeat the Following Cards NMODES Times

(6I12) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM1(i)	NFI				
Item	(1)	(2)				

- (1) NTM1(i) Number of deformation mode coefficients for the wing, mode i  
 (2) NFI Compute generalize forces; 0 ~ No, 1 ~ Yes  
 If NFI = 0 the program will compute the VPIC's and stop.

## (6E12.5) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	CØ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

(1) CØ(1)

$i = 1$ , NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; where the first integer is the power of "x" and the second is the power of "y". Continue on successive cards until all polynomial coefficients are input.

## (6I12) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM	NFI				
Item	(1)	(2)				

(1) NTM2(1)

Number of deformation mode coefficients for the control surface, mode (i)

(2) NFI

Compute generalized forces; 0 ~ No; 1 ~ Yes. If NFI = 0, the program will compute the VPIC's and stop.

## (6E12.5) Format

Column	1-12	13-24	25-36	37-48	49-60	
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	
Item	(1)	(2)	(3)	(4)	(5)	

CØ(i)

$i = 1$ , NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; etc. where the first integer is the power of "x" and the second is the power of "y". Continue on successive cards until all polynomial coefficients are input.

#### 4.4 SAMPLE PROBLEM

The generalized forces are calculated for the configuration below. The flight parameters and pertinent input data are presented on the first page of the computer print out.

The coefficients of the deformation modes for the forward surface are shown on the third page of the computer print out, and for the aft surface on the fifth page of the computer print out.

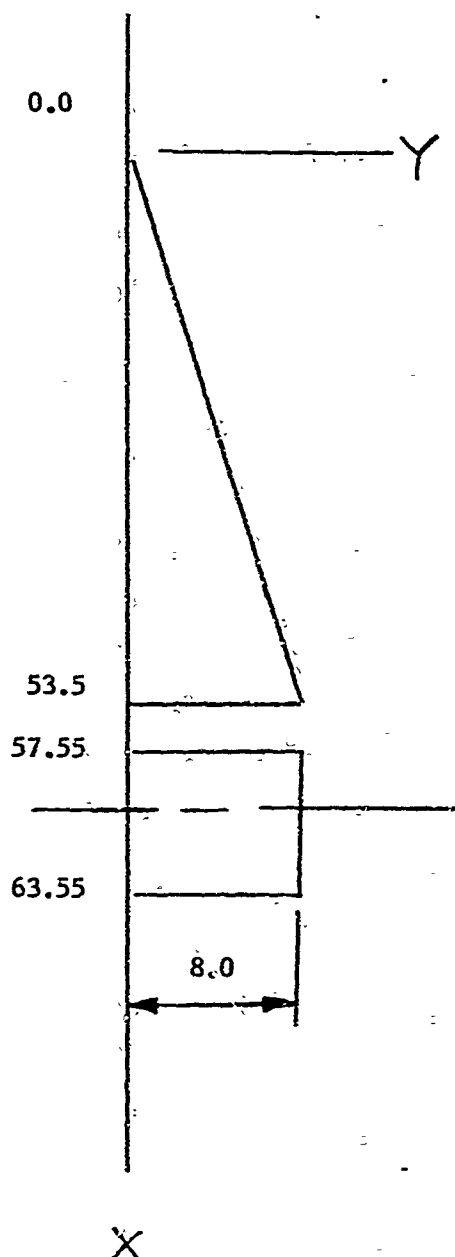


FIGURE 4.4.1

# HAC/NAA MISSILE TRANSONIC AIRLOADS PROGRAM

## FLIGHT CONDITIONS AND GEOMETRY

MACH NUMBER = 1.00000 SPEED OF SOUND = 13392.000 L/T RHO = 0.11460000E-06

	WING	TAIL
L.E. STATION (L)	0.	57.550
ROOT CHORD (L)	53.500	6.000
L.E. SPAN (L)	0.	8.000
T.E. SPAN (L)	8.000	6.000
TIP CHORD (L)	0.	6.000
TOTAL AREA (L+L)	428.000	96.000
CHORDWISE BOXES	49	5
SPANWISE BOXES	7	7

TOTAL CHORDWISE BOXES = 53 BOX CHORD = 1.20225E 00 L BOX SPAN = 1.20225E 00 L

HAP OF SONIC RUX OVERLAY  
ON WING, TAIL AND WAKE  
(S) - WING  
(S) - TAIL  
(S) - WAKE

[illegible]

# MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GHS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR WING  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE	COEFFS.									
1	6.2231E-01	4.6476E-03	2.1714E 00	-1.1796E-02	1.1765E-01	-2.3426E 00	1.3893E-03			
	-5.7624E-02	7.9094E-01	-2.5125E 00	-4.5847E-05	2.4591E-03	-3.5940E-02	1.4666E-01			
	-9.2425E-02	4.4647E-07	-2.7338E-05	4.4296E-04	-2.5737E-03	7.8341E-03	-1.7714E-02			
2	8.9494E-04	-1.4724E-03	-1.5229E-02	1.3060E-04	1.4047E-03	2.5887E-02	-1.7714E-00			
	-3.0455E-04	1.0010E-03	-1.8106E-02	-5.8051E-08	1.4540E-05	-1.7126E-04	1.5541E-03			
	-1.9612E-03	1.0317E-09	-1.6695E-07	2.2909E-06	-1.3876E-05	-3.8650E-05	2.1062E-04			
3	-2.0277E-03	-1.8600E-03	-4.0090E-01	2.8498E-03	-5.4255E-02	5.2506E-01	-3.2033E-04			
	1.5004E-02	-1.7053E-01	5.3718E-01	1.0353E-05	-6.0834E-04	7.9328E-03	-3.2827E-02			
	2.2924E-02	-1.0013E-07	6.6433E-06	-9.9828E-05	8.9923E-04	-1.9292E-03	4.73643E-03			
4	6.8155E-03	-6.2155E-03	-1.0847E 00	2.4746E-03	9.3898E-02	4.8655E-01	-2.3470E-04			
	2.7715E-03	-1.1654E-01	3.2703E-01	7.1836E-06	-2.3984E-04	5.1428E-03	-2.1053E-02			
	1.9833E-02	-6.7781E-08	3.0791E-06	-6.1616E-05	3.4012E-04	-8.7292E-04	1.4206E-03			
5	2.2147E-03	9.1320E-04	1.8393E-03	-6.5138E-04	1.7097E-02	-8.4167E-02	6.8571E-05			
	3.3292E-03	3.8491E-02	-1.3252E-01	-2.1796E-06	1.3006E-04	-1.7763E-03	7.4320E-03			
	-3.9610E-03	2.0953E-08	-1.3987E-06	2.1637E-05	-1.2205E-04	3.2906E-04	-7.4633E-04			

# MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.00000 53 BOXES IN CHORD DIRECTION  
REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

GENERALIZED FORCES FOR WING					
DEFL	LOAD	REAL PART	IMAG. PART	ABS VALUE	PHASE ANGLE
1	1	3.16858E 02	-1.37658E 02	3.45499E 02	-23.482 DEG
1	2	-5.52591E-01	2.66777E 00	2.72440E 00	101.703 DEG
1	3	-5.62170E 01	2.07533E 01	5.99254E 01	159.738 DEG
1	4	-8.10722E 00	3.26216E 01	3.36139E 01	103.957 DEG
1	5	1.18660E 01	-6.65916E 00	1.34328E 01	-28.719 DEG
2	1	-2.44226E 00	2.26683E 00	3.33234E 00	137.133 DEG
2	2	8.84216E-01	-2.39821E-01	9.16162E-01	-15.175 DEG
2	3	-5.69430E 00	2.64395E 00	6.27818E 00	155.094 DEG
2	4	-1.55191E 00	-2.19162E 00	2.68545E 00	-125.303 DEG
2	5	2.87546E-01	-2.50006E-02	2.88631E-01	-4.969 DEG
3	1	-6.65830E 01	2.52397E 01	7.12063E 01	159.240 DEG
3	2	-7.04967E 00	-1.50816E 00	7.20919E 00	-167.923 DEG
3	3	7.38453E 01	-1.35683E 01	7.50815E 01	-10.411 DEG
3	4	2.91514E 01	1.99798E 01	3.53412E 01	34.426 DEG
3	5	-7.90048E 00	-2.34433E-01	7.90395E 00	-178.300 DEG
4	1	1.59553E 01	2.36006E 01	2.84879E 01	55.939 DEG
4	2	-2.71097E 00	3.88001E 00	4.73326E 00	124.942 DEG
4	3	3.77450E 00	-3.69283E 01	3.71207E 01	-84.164 DEG
4	4	-2.14405E 01	-1.64663E 01	2.70339E 01	-112.476 DEG
4	5	2.92952E 00	5.23504E 00	6.02850E 00	60.271 DEG
5	1	6.76158E 00	-7.51507E 00	1.01092E 01	-48.021 DEG
5	2	5.48742E-01	-3.20824E-01	6.35646E-01	-30.313 DEG
5	3	-4.27173E 00	4.95884E 00	6.54506E 00	130.743 DEG
5	4	4.30316E 00	2.14755E 00	4.80928E 00	26.522 DEG
5	5	1.87838E-01	-9.02441E-01	9.21783E-01	-78.242 DEG



# MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR TAIL  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

## COEFFS.

MODE	COEFFS.
1	-1.0091E-00 3.6669E-02 2.0342E-02 2.5379E-02 2.2663E-03 -6.3951E-03 -3.9767E-03 -2.0287E-03 9.8702E-04 1.1172E-03 1.9252E-04 3.7068E-04 -2.0327E-04 1.7562E-06 -6.7077E-05
2	-1.2752E-01 8.2139E-02 -8.3996E-02 -1.7451E-02 -2.6948E-02 -2.0262E-02 1.2913E-03 7.7354E-03 1.6668E-03 2.9726E-03 3.1356E-05 -2.7508E-04 -5.4809E-04 1.6180E-05 -1.0213E-04
3	-8.3787E-02 4.9086E-02 -8.5200E-03 -1.6733E-02 -1.4954E-03 -1.2620E-03 4.0742E-03 1.5179E-05 2.7897E-04 2.8296E-04 -3.1325E-04 4.5623E-06 -6.0549E-07 -1.7126E-05 -1.9476E-05
4	-7.2257E-03 8.2141E-03 -4.9131E-03 -1.1390E-03 -2.5330E-04 7.4449E-04 9.5326E-05 1.7613E-05 -3.0224E-06 -2.4853E-04 1.6233E-07 1.5745E-05 -2.1877E-05 1.2826E-05 1.7159E-05
5	5.8014E-01 1.5199E-01 2.4793E-02 8.4246E-02 5.0903E-03 -1.8510E-02 -1.9336E-02 -9.6255E-05 4.2392E-05 3.4434E-03 1.3989E-03 -1.1667E-04 5.2220E-05 -1.5344E-05 -2.0522E-04

# MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.0000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.38055 FREE STREAM MACH NUMBER 1.000

## GENERALIZED FORCES FOR TAIL

DEFL	LOAD	REAL PART	IMAG PART	ABS VALUE	PHASE ANGLE
1	1	3.20570E 02	-1.64106E 02	3.60133E 02	-27.109 DEG
1	2	1.78757E 02	-1.52739E 02	2.35104E 02	-47.507 DEG
1	3	1.35618E 02	-3.12913E 01	1.39181E 02	-12.992 DEG
1	4	1.40816E 02	-6.58142E 01	1.55437E 02	-25.050 DEG
1	5	1.03474E 03	-7.16951E 01	1.03722E 03	-3.964 DEG
2	1	1.65340E 02	-8.80348E 01	1.87316E 02	-28.033 DEG
2	2	1.24794E 02	-9.42639E 01	1.56393E 02	-37.065 DEG
2	3	8.75103E 01	-1.55398E 01	8.88793E 01	-13.069 DEG
2	4	9.66705E 01	-3.27417E 01	1.02045E 02	-18.711 DEG
2	5	5.96996E 02	6.51462E 00	5.97032E 02	0.625 DEG
3	1	1.17162E 01	-2.23677E 01	2.52681E 01	-67.376 DEG
3	2	1.64673E 00	-1.09465E 01	1.10696E 01	-81.445 DEG
3	3	1.07777E 01	-6.32983E 00	1.24990E 01	-30.426 DEG
3	4	1.24434E 01	-6.77398E 00	1.41673E 01	-28.560 DEG
3	5	8.18177E 01	-4.11626E 01	9.19887E 01	-26.707 DEG
4	1	1.29545E 00	-4.67734E 00	4.85313E 00	-74.518 DEG
4	2	8.41320E 01	-2.50315E 00	2.64076E 00	-71.422 DEG
4	3	2.58365E 00	-1.28241E 00	2.88441E 00	-26.398 DEG
4	4	3.05965E 00	-1.28912E 00	3.32013E 00	-22.847 DEG
4	5	1.71697E 01	-7.84607E 00	1.88775E 01	-24.559 DEG
5	1	1.23287E 02	-1.61959E 02	2.03545E 02	-127.279 DEG
5	2	1.78991E 02	5.78304E 00	1.79084E 02	178.149 DEG
5	3	-2.08674E 00	-5.89137E 01	5.89507E 01	-92.029 DEG
5	4	3.43775E 00	-3.42119E 01	3.43842E 01	-84.262 DEG
5	5	1.29038E 02	-5.72898E 02	5.87251E 02	-77.507 DEG

# MISSILE TRANSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 110.00000 53 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD): 1.38055 FREE STREAM MACH NUMBER 1.000

## GENERALIZED FORCES FOR WING + TAIL

DEFL	LOAD	REAL PART	IMAG PART	ABS VALUE	PHASE ANGLE
1	1	6.37428E 02	-3.01764E 02	7.05249E 02	-25.333 DEG
1	2	1.78204E 02	-1.50041E 02	2.32957E 02	-40.096 DEG
1	3	7.94010E 01	-1.05381E 01	8.00972E 01	-7.560 DEG
1	4	1.32709E 02	-3.31926E 01	1.36797E 02	-14.042 DEG
1	5	1.04641E 03	-7.83542E 01	1.04934E 03	-4.282 DEG
2	1	1.62898E 02	-8.57680E 01	1.84097E 02	-27.767 DEG
2	2	1.25678E 02	-9.45007E 01	1.57243E 02	-36.940 DEG
2	3	8.18160E 01	-1.28959E 01	8.28261E 01	-8.957 DEG
2	4	9.51186E 01	-3.49333E 01	1.01331E 02	-20.166 DEG
2	5	5.97284E 02	6.48962E 00	5.97319E 02	0.623 DEG
3	1	5.48668E 01	2.85198E 00	5.49409E 01	177.024 DEG
3	2	5.40294E 00	-1.24546E 01	1.35761E 01	-113.452 DEG
3	3	8.46230E 01	-1.98982E 01	8.69310E 01	-13.232 DEG
3	4	4.15948E 01	1.32068E 01	4.36411E 01	17.615 DEG
3	5	7.39172E 01	-4.13970E 01	8.47200E 01	-29.251 DEG
4	1	1.72507E 01	1.89236E 01	2.56064E 01	47.648 DEG
4	2	1.86965E 00	1.37685E 00	2.32192E 00	143.631 DEG
4	3	6.35815E 00	-3.82107E 01	3.87361E 01	-80.553 DEG
4	4	1.63808E 01	-1.77554E 01	2.55560E 01	-135.992 DEG
4	5	2.01593E 01	-2.61103E 00	2.03276E 01	-7.380 DEG
5	1	1.16525E 02	-1.69474E 02	2.05669E 02	-124.511 DEG
5	2	1.78442E 02	5.46221E 00	1.78526E 02	178.247 DEG
5	3	6.38847E 00	-5.39549E 01	5.43283E 01	-96.721 DEG
5	4	7.74090E 00	-3.20643E 01	3.29855E 01	-76.427 DEG
5	5	1.29226E 02	-5.73801E 02	5.88172E 02	-77.308 DEG

# 4.5 PROGRAM LISTING

```

*      FORTRAN NESTON, DECK                                SON70030
CISIS      CSIS                                             SON70050
BLOCK DATA                                              SON70060
COMPLEX CZERO, PHI, PHIE, DPHI, SPHI                    SON70070
COMMON/C3/C(10,24,2), N1(10,2), NF(10,2), NTHAX(2), FN(28), DXE(6), TP SON70080
COMMON/C7/CZERO, PHI, PHIE, DPHI, SPHI                  SON70090
COMMON/C8/RND                                             SON70100
DATA CZERO/(0.0,0.0)/, TP1/6.2831853/, FN/0.,1.,0.,2.,1.,0.,3.,2., SON70110
1 1.,0.,4.,3.,2.,1.,0.,5.,4.,3.,2.,1.,0.,6.,5.,4.,3.,2.,1.,0./ SON70120
END                                                       SON70130
*      FORTRAN NESTON, D-CK                                SON70140
CPAIN      MAIN                                           SON70160
COMPLEX VPI, DS, DQ, Q, PHIW, CK, CZERO, PHI, PHIE, DPHI, SPHI, ASU, EXF SON70170
DIMENSION ASQ(40,40)                                     SON70180
COMMON/C1/K: OX(2000), XE(5), YE(3), AR(3), X1, X2, X3, X4, Y1, Y2, BETA, NBS SON70190
COMMON/C2/AN, MAC=1, FACH(6), NREQ, FREQ(10), NMODE, NSURF, LVPIC, LSSVP SON70200
COMMON/C3/C(10,24,2), N1(10,2), NF(10,2), NTHAX(2), FN(28), DXE(6), TP SON70210
COMMON/C4/VPI(20,15), DS(2000), DQ(28,2), Q(10,10,3), PHIW(50), CK(40) SON70220
COMMON/C5/MOD(100), BRL(100), FC, IFR, XL, NS, NIM, K, J, QR, QI, QAB, QAN SON70230
COMMON/C6/X, Y, DX, DY, EX, EK, EKB, EKR, NP, PP, NB, NBOX, KODE, MODE, NBW, NBT SON70240
COMMON/C7/CZERO, PHI, PHIE, DPHI, SPHI                  SON70250
COMMON/C8/RND                                             SON70260
1 CALL MAIN                                              SON70270
DO 1000 MAC=1, MACN                                     SON70280
  FC = FACH(FACH)                                       SON70290
  IF(ABS(FC-1.0).GT.0.05) GO TO 1000                    SON70300
  CALL CDEF                                             SON70310
  CALL POUT(1)                                           SON70320
  TP1=TP1/(AS*F1)                                       SON70330
  RFN = DX                                              SON70340
  DO 900 IFR = 1, NREQ                                  SON70350
    FK=FRFQ(IFR)*TP1                                     SON70360
    IF(FK.EQ.0.0) GO TO 900                             SON70370
    FRF = FK*RFN                                         SON70380
    FRD = FK*X1/2.0                                     SON70390
    CALL POUT2H                                          SON70400
    IF(LVPIC.NE.0) CALL POUT(2)                         SON70410
    ARG=FK*DX                                             SON70420
    EXF=CMPLX(COS(ARG), -SIN(ARG))                     SON70430
    DO 500 MDE=1, NMODE                                  SON70440
      DO 10 J=1,5                                        SON70450
        DQ(J,1)=CZERO                                   SON70460
        IF(MDE(MDE,1).EQ.0) GO TO 210                  SON70470
        X=0.5*DX                                         SON70480
        NB=J                                              SON70490
        IF(LSSVP.NF.0) CALL POUT(3)                    SON70500
        DO 200 NP=1, NBOX                               SON70510
          PR=MOR(NP)                                     SON70520
          Y=0.0                                           SON70530
          KODE = KBOX(NB)                                SON70540
          NS = 1                                          SON70550
          GO TO (12,11,12,11,11,120), KODE             SON70560
11      NS = 2                                          SON70570
12      DO 20 MP=1, B                                    SON70580
          SPH1 = CZERO                                    SON70600
          IF(MP.GT.1) CALL PHIR                         SON70610
          CALL WASH                                       SON70620
          CK(MP)=DS(NB)                                  SON70630
          DS(MP) = DS(NB) - SPH1                       SON70640
          Y = Y+BY                                       SON70650

```

```

20 NB = NB+1
   NB = NB-MB
   DO 30 IU=1,MB
   DO 30 JU=1,MB
   IJU = IABS(IU-JU)+1
25 ASQ(IU,JU) = VPIC(IJU,1)
   IF(JU.EQ.1) GO TO 30
   IJU=IU+JU-1
   ASQ(IU,JU)=ASQ(IU,JU)+VPIC(IJU,1)
30 CONTINUE
   ISQ = MSIMEC(40,MB,1,ASQ,DS(NB))
   IF(ISQ.EQ.1) GO TO 39
   CALL POUT(8)
   GO TO 900
39 CONTINUE
   Y = 0.0
   IF(OP.NE.1) GO TO 50
   DO 45 MP=1,MB
45 DS(MP) = DS(MP)*2.0*3.1415927
50 CONTINUE
   IF(KODE.NE.4) GO TO 80
   DO 60 MP=1,MB
   DS(MP) = PHIW(MP)*(DS(NB)-PHIW(MP))*2.0*3.1415927
60 NB=MB+1
   NB=NB-MB
80 CONTINUE
   DO 100 MP=1,MB
   IF(KODE.EQ.3) PHIW(MP)=DS(NB)*EXF
   IF(LP.FQ.NBOX-1) PHIW(MP)=DS(NB)
   PHIE = DS(NB)
   IF(MP.FQ.NBOX) PHIE = PHIE+(PHIE-PHIW(MP))*DXE(5)
   PHI = DS(NB)
   IF(ISSVP.NE.0) CALL POUT(4)
   CALL DQIU
   NB = NB + 1
100 Y=Y+DY
   GO TO 200
120 DO 130 MP=1,MB
   DS(MP)=PHIW(MP)
   PHIK(MP) = EXF*PHIW(MP)
   CK(MP)=CZERO
   IF(ISSVP.NE.0) CALL POUT(4)
130 NB = NB+1
200 X = X+DX
210 DO 400 MO = 1,MODE
   DO 300 NS=1,NSURF
   Q(MODE,MO,NS)=CZERO
   NTM=NT(MO,NS)
   DO 300 N=1,IM
300 Q(MODE,MO,NS)=Q(MODE,MO,NS)+CU(MO,N,NS)*DQ(N,NS)
   Q(MODE,MO,3) = CZERO
400 Q(MODE,MO,3)=Q(MODE,MO,1)+Q(MODE,MO,2)
500 CONTINUE
   DO 800 NS=1,3
   CALL POUT(6)
   DO 700 J=1,MODE
   DO 700 K=1,MODE
   QR = FQ*REAL(Q(K,J,NS))
   QI = FQ*AIMAG(Q(K,J,NS))
   CAP=SQR(QI*QI+QR*QR)

```

SON70660  
SON70670  
SON70680  
SON70690  
SON70700  
SON70710  
SON70720  
SON70730  
SON70740  
SON70750  
SON70760  
SON70770  
SON70780  
SON70790  
SON70800  
SON70810  
SON70820  
SON70830  
SON70840  
SON70850  
SON70860  
SON70870  
SON70880  
SON70890  
SON70900  
SON70910  
SON70920  
SON70940  
SON70950  
SON70960  
SON70970  
SON70980  
SON70990  
SON71000  
SON71010  
SON71020  
SON71030  
SON71040  
SON71060  
SON71070  
SON71080  
SON71090  
SON71100  
SON71110  
SON71120  
SON71130  
SON71140  
SON71150  
SON71160  
SON71170  
SON71180  
SON71190  
SON71200  
SON71210  
SON71220  
SON71230  
SON71240  
SON71250  
SON71260  
SON71270

```

      QAN=0.0
      IF (QAB.NE.0.0) QAN=57.29578*ATAN2(QI,QR)
700  CALL PCUL(7)
      IF (NSURF.EQ.1) GO TO 900
800  CONTINUE
900  CONTINUE
1000 CONTINUE
      GO TO 1
      END

$      FORTRAN NLSTOU,DECK
CHAIN      DAIN
      SUBROUTINE DAIN
      COMMON/C1/KNOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
      COMMON/C2/AS,MACH,MACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP
      COMMON/C3/CI(10,28,2),NT(10,2),NF(10,2),NTMAX(2),FN(28),DXE(6),TPI
      COMMON/C6/X,Y,DX,DY,FX,EK,EKB,EKR,NP,PP,NB,NBOX,KODE,MODE,NBW,NBI
      COMMON/C8/RHO
      READ(5,11) (XF(I),I=1,5)
      READ(5,11) (YE(I),I=1,3),AS,RHO
      RHO = RHO/1000.
      READ(5,12) MACH,NFREQ,NMODE,NBW,LVPIC,LSSVP
      READ(5,11) (FMACH(I),I=1,NMACH)
      READ(5,11) (FREQ(I),I=1,NFREQ)
      NSURF=2
      IF (XF(4).LT.XF(5)) GO TO 10
      NSURF=1
      XF(4)=XL(3)
      YE(5)=XE(3)
10  NTMAX(1)=0
      NTMAX(2)=0
      DO 30 MODE=1,NMODE
      DO 30 I=1,NSURF
      DO 20 J=1,2
20  CO(MODE,J,1)=0.
      READ(5,12) TM,CFI
      NT(MODE,1)=TM
      NTMAX(1)=MAX0(NTMAX(1),NTM)
      NF(MODE,1)=CFI
30  READ(5,11) (CO(MODE,J,1),J=1,NTM)
11  FORMAT(6E12.8)
12  FORMAT(6I12)
      RETURN
      END

$      FORTRAN NLSTOU,DECK
CCCCF      CODE
      SUBROUTINE CODE
      COMMON/C1/KNOX(2000),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
      COMMON/C2/AS,MACH,MACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP
      COMMON/C3/CI(10,28,2),NI(10,2),NF(10,2),NTMAX(2),FN(28),DXE(6),TPI
      COMMON/C5/MFB(100),NBL(100),FU,IFR,XL,NS,NTM,K,J,QR,QI,QAB,QAN
      COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,PP,NB,NBOX,KODE,MODE,NBW,NBI
      COMMON/C8/RHO
      BETA = EM
      X1 = XF(3) - XF(1)
      X2 = XF(3) - XF(2)
      X3 = XE(4) - XF(1)
      X4 = XF(5) - XF(4)
      X5 = XE(5) - XF(1)
      Y1 = YE(2) - YE(1)
      Y2 = YE(3) - YE(1)

```

SON71280  
SON71290  
SON71300  
SON71310  
SON71320  
SON71330  
SON71340  
SON71350  
SON71360  
SON71370  
SON71390  
SON71400  
SON71410  
SON71420  
SON71430  
SON71440  
SON71450  
SON71460  
SON71470  
SON71480  
SON71490  
SON71500  
SON71510  
SON71520  
SON71530  
SON71540  
SON71550  
SON71560  
SON71570  
SON71580  
SON71590  
SON71600  
SON71610  
SON71620  
SON71630  
SON71640  
SON71650  
SON71660  
SON71670  
SON71680  
SON71690  
SON71700  
SON71710  
SON71720  
SON71740  
SON71750  
SON71760  
SON71770  
SON71780  
SON71790  
SON71800  
SON71810  
SON71820  
SON71830  
SON71840  
SON71850  
SON71860  
SON71870  
SON71880  
SON71890

```

IF(X2.GT.X1.OR.X1.GT.X3.OR.X3.GT.X5.OR.X2.LT.0.0) GO TO 50
IF(Y1.GT.Y2.OR.Y1.LT.0.0) GO TO 50
TWL = 0.0
IF(Y2.NE.Y1) TWL = (X1 - X2) / (Y2 - Y1)
AR(1) = (Y2*(X2+X1) - Y1 * (X2-X1))
AR(2) = Y2*X4*2.0
AR(3) = AR(1) + AR(2)
10 DX = X1/(FL*AT(NBW) - 0.5)
IF (100.0* DX .GT. X5) GO TO 20
15 NBW = NBW-1
GO TO 10
20 DY = DX/BETA
YH1 = Y1/DY
YH2 = Y2/DY
XN1 = YH2 - (X1-X2) / DX
XN1 = YH2 + X5/DX
XN1F = X3/DX
XN1F = X5/DX
NBWX = XN1F + 0.5
NBS = Y2/DY + 1.0
NBT = X4/DX + 0.5
DXF(1) = 1.0
DXF(2) = 1.0
DXF(3) = 0.5
DXF(4) = ATN(XN1F + 1.5) - XN1F
DXF(5) = XN1F - FL*AT(NBWX-1)
DXF(6) = 0.5
X = 0.5 * DX
NB = 0
KODE = 1
DO 40 NP = 1,NB*DX
XN = FL*AT(NP) - 0.5
YH = YH2
IF (TWL .GT. 0.0) YH=AMIN1(YH,YN1+XN/(TWL/BETA))
MH = IFIX(YH)+1
28 MUR(NP) = MH
IF(MB.GT.40) GO TO 15
IF (NP .EQ. NBW) KODE = 3
IF (NSURF .EQ. 1) GO TO 29
IF (X .GT. x1) KODE = 6
IF (X .GT. x3) KODE = 4
IF (X .GT. x3+DX) KODE = 2
IF (NP .EQ. NBWX) KODE = 5
29 IF(MB+MB.GT.2000) GO TO 15
MBI(NP) = MB
DO 30 MP = 1,MB
NB = NB + 1
30 KBOX (NB) = KBOX
40 X = X+DX
QORHO = 0.5*(AS*E4)**2
FO = -6.0*DX*DY*QORHO/EM*RHU
RETURN
50 CALL EXPI
RETURN
END

```

SON71900  
SON71910  
SON71920  
SON71930  
SON71940  
SON71950  
SON71960  
SON71970  
SON71980  
SON71990  
SON72000  
SON72010  
SON72020  
SON72030  
SON72040  
SON72050  
SON72060  
SON72070  
SON72080  
SON72090  
SON72100  
SON72110  
SON72120  
SON72130  
SON72140  
SON72150  
SON72160  
SON72170  
SON72180  
SON72190  
SON72200  
SON72210  
SON72220  
SON72230  
SON72240  
SON72250  
SON72260  
SON72270  
SON72280  
SON72290  
SON72300  
SON72310  
SON72320  
SON72330  
SON72340  
SON72350  
SON72360  
SON72370  
SON72380  
SON72390  
SON72400  
SON72410  
SON72420  
SON72430  
SON72440  
SON72450  
SON72470  
SON72480  
SON72490  
SON76460

COMMON/C5/MOR(100),MRL(100),FU	IFR,XL,NS,NTM,K,J,QR,QT,QAB,QAN	SUN72510
COMMON/C6/X,Y,DX,DY,EH,EK,EKB,EKR,NP,PP,ND,NBOX,KODE,MODE,NBW,NBT		SUN72520
COMMON/C8/RHO		SUN72530
K=2*MOR(NBOX)		SUN72540
N=MIND(NBOX,15)		SUN72550
DK=EK8		SUN72560
DK2=DK**2		SUN72570
K1=K-1		SUN72580
DKR=DK2/8.0		SUN72590
DK4=2.0*DK8		SUN72600
DK12=DK2/12.0		SUN72610
CH=0.5		SUN72620
DM=DK*0.5		SUN72630
DM=0.5*DM		SUN72640
DD=2.0*DK		SUN72650
DDM=DD		SUN72660
D1=0.25*DK2		SUN72670
B5=DK2/24.0		SUN72680
B6=1.0		SUN72690
B1=0.0		SUN72700
B4=2.0/DM		SUN72710
B2=B5/B4-DM		SUN72720
B3=-0.5*B5		SUN72730
B5=DM*B4+B5		SUN72740
D4=DK8*B4		SUN72750
DD4=2.0*B4		SUN72760
CN=1.0		SUN72770
C3=0.0		SUN72780
C4=0.0		SUN72790
C7=0.0		SUN72800
CR=0.0		SUN72810
DO 2 J=1,N		SUN72820
A1=DM/CH		SUN72830
C1=CM* COS(A1)		SUN72840
C2=-CM* SIN(A1)		SUN72850
CALL CSIN(A1,C5,C6)		SUN72860
C5=CM*C5		SUN72870
C6=-CM*C6		SUN72880
C9=C1-C3		SUN72890
C10=C2-C4		SUN72900
C11=C5-C7		SUN72910
C12=C6-C8		SUN72920
VRF=B3*C9-B4*C10-B5*C3-B1*C11-B2*C12		SUN72930
VIM=B4*C9+B3*C10-B5*C4+B2*C11-B1*C12		SUN72940
VPIC(I,J)=C*PI X(VRF,VIM)		SUN72950
23 C3=C1		SUN72960
C4=C2		SUN72970
C7=C5		SUN72980
CH=C6		SUN72990
B1=B1-B1		SUN73000
B3=B3-B3		SUN73010
B4=B4-B4		SUN73020
B4=B4+DD4		SUN73030
CN=CN+2.0		SUN73040
2 CGN=1/NOE		SUN73050
CM=CM+1.0		SUN73060
DM=DM+DDM		SUN73070
3 DDM=DDM+DD		SUN73080
DO 5 J=1,N		SUN73090
DO 4 I=1,M1		SUN73100



```

3 K=M-1
4 VPIC(K+1,J)=VPIC(K+1,J)-VPIC(K,J)
5 VPIC(1,J)=2.0*VPIC(1,J)
  CM=0.0
  DM=0.0
  DDM=DK
  DO 12 I=1,M
    C7=0.0
    C8=0.0
    C9=0.0
    C10=0.0
    P1=0.0
    P2=0.0
    CH=1.0
    H6=0.5*DK12
    DO 10 J=1,N
      A1=CM/CN
      A2=DM/CN
      IF (A1-0.2) 7,7,8
7 R1=2.0-A1**2/3.0
      R2=-DK/(6.0*CH)
      GO 10 9
8 B3= SIN(A1)/A1
      R1=2.0*B3
      R2=(B3- COS(A1))/12-DH/CN*B3
9 B3= COS(A2)/CN
      B4= SIN(A2)/CN
      C3=B1*B3+B2*B4
      C4=B2*B3-B1*B4
      B5=DH*CN
      C1=1.5*C4-2.0*C3
      C2=-2.0*C4+1.5*C3
      C5=C1-C7
      C6=C2-C8
      P3=P2-R6*CN
      P4=B3+2.0*DH12*(C1-1.0)
      VRE=C5-P1*C6+P3*C3-P4*C9
      VIM=C6+P1*C5+P3*C4-P4*C10
      VPIC(1,J)=VPIC(1,J)+CMPLX(VRE,VIM)
      P1=P1+DH
      P2=P2+CN*DK4
      CN=CN+2.0
      C7=C1
      C8=C2
      C9=C3
      C10=C4
      B6=B5+DK12
10 CONTINUE
  CM=CM+DK
  DM=DM+DDM
12 DDM=DDM+DD
  D3=DK/(2.0*3.14159265)
  A1=0.0
  DO 14 J=1,N
    CEX=D3*CMPLX(SIN(A1), COS(A1))
    DO 13 I=1,M
13 VRE=C(1,J)+CEX*VPIC(I,J)
14 A1=A1+DH
  RETURN
  END

```

```

SON73110
SON73120
SON73130
SON73140
SON73150
SON73160
SON73170
SON73180
SON73190
SON73200
SON73210
SON73220
SON73230
SON73240
SON73250
SON73260
SON73270
SON73280
SON73290
SON73300
SON73310
SON73320
SON73330
SON73340
SON73350
SON73360
SON73370
SON73380
SON73390
SON73400
SON73410
SON73420
SON73430
SON73440
SON73450
SON73460
SON73470
SON73480
SON73490
SON73500
SON73510
SON73520
SON73530
SON73540
SON73550
SON73560
SON73570
SON73580
SON73590
SON73600
SON73610
SON73620
SON73630
SON73640
SON73650
SON73660
SON73670
SON73680
SON73690
SON73700

```

1	FORTRAN NLSTOU,DECK	SUN73710
CCSIN	CSIN	SUN73730
	SUBROUTINE CSIN(X),U,S)	SUN73740
C	SINE AND COSINE INTEGRAL SUBROUTINE	SUN73750
C		SUN73760
C	C AND S ARE THE INTEGRALS OVER T FROM 1 TO INFINITY OF	SUN73770
C	COS(XT)/T AND SIN(XT)/T	SUN73780
C		SUN73790
	SG=1.0	SUN73800
	X=X1	SUN73810
	IF (X) 1,2,2	SUN73820
1	SG=-SG	SUN73830
	X=-X	SUN73840
2	X2=X*X	SUN73850
	IF (X-1.0) 3,3,4	SUN73860
C		SUN73870
C	FOR ABS(X) LESS THAN 1 A SERIES EXPANSION IS USED	SUN73880
C		SUN73890
1	V=((X2/98.0-0.6)*.05*X2+1.0)*X2/18.0-1.0)*X+1.57079633	SUN73900
	L=((X2/45.0-1.0)*X2/24.0+1.0)*X2/4.0-.577215665-ALOG(X)	SUN73910
	GO TO 5	SUN73920
C		SUN73930
C	FOR ABS(X) GREATER THAN 1 APPROXIMATIONS OF HASTINGS ARE USED	SUN73940
C		SUN73950
1	P=((X2+19.194119)*X2+47.411538)*X2+8.493336)/((((X2+21.361055)	SUN73960
1	*X2+70.375496)*X2+30.038227)*X)	SUN73970
	Q=((X2+21.383724)*X2+49.719775)*X2+5.089504)/((((X2+27.177958)	SUN73980
1	*X2+119.918932)*X2+76.707876)*X2)	SUN73990
	CO=COS (X)	SUN74000
	SI=SIN (X)	SUN74010
	I=0*CO-P*SI	SUN74020
	V=P*CO+0*SI	SUN74030
5	S=V*SG	SUN74040
	RETURN	SUN74050
	END	SUN74060
1	FORTRAN NLSTOU,DECK	SUN74070
CRASH	WASH	SUN74090
	SUBROUTINE WASH	SUN74100
	COMPLEX VPIC,DS,DQ,0,PHIW,CK	SUN74110
	COMMON/C1/KIOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS	SUN74120
	COMMON/C3/CI(10,28,2),NI(10,2),NF(10,2),NIMAX(2),FN(28),DXE(6),TPI	SUN74130
	COMMON/C4/VPIC(40,15),DS(2000),DQ(28,2),Q(10,10,3),PHIW(50),CK(40)	SUN74140
	COMMON/C5/MOQ(100),NRL(100),FQ,IFR,XI,NS,NIM,K,J,OR,UI,QAB,QAN	SUN74150
	COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,PP,NR,NBOX,KODE,MODE,NBW,NBT	SUN74160
	COMMON/C8/RHO	SUN74170
	XP = X	SUN74180
	IF (NS.EQ.2) XP = X - X3	SUN74190
	NIM = NI(MODE,NS)	SUN74200
	Z = CO(MODE,1,NS)	SUN74210
	DZ = 0.0	SUN74220
	IF (NIM.EQ.1) GO TO 70	SUN74230
	K = 1	SUN74240
	IF (XP.EQ.0.0) GO TO 50	SUN74250
	PX = XP	SUN74260
	YX = Y/XP	SUN74270
	DO 40 N=2,7	SUN74280
	PXY = PX	SUN74290
	DO 30 M = 1,N	SUN74300
	K = K + 1	SUN74310
	IF (K.GT.NIM) GO TO 20	SUN74320

```

      ZP=PX*Y*CO(MODE,K,NS)
      7=7+ZP
      DZ=DZ+EX(K)*ZP
30  PX=PX*YX
40  PY=PY*XP
20  DZ=DZ/XP
      GO TO 70
50  PX=1.0
      DO 60 N=2,7
      K=K+N
      KK=K-1
      IF(KK.LE.NT) DZ=DZ+PX*CO(MODE,KK,NS)
      PX=PX*Y
      IF(K.GT.NT) GO TO 70
60  7=7+PX*CO(MODE,K,NS)
70  GO TO (80,90),NS
80  DS(MR) = CMPLX(DZ,EK*Z)
      RETURN
90  DS(MR) = CMPLX(-DZ,EK*Z)
      RETURN
      END
$      FORTRAN NLSTOU,DECK
CPHIB      PHIB
      SUBROUTINE PHIB
      COMPLEX VPIC,DS,DU,C,PHIW,CK,CZIRO,PHI,PHITE,DPHI,SPHI
      COMMON/C4/VPIC(40,15),DS(2000),DU(28,2),C(10,10,3),PHIW(50),CK(40)
      COMMON/C5/MOR(100),LBL(100),FU,IFR,XL,NS,NTM,K,J,QR,QI,QAB,QAN
      COMMON/C6/X,Y,PA,JY,EM,EK,EKB,EKR,NP,MP,NB,NBUX,KODE,MODE,NBW,NBT
      COMMON/C7/CZIRO,PHI,PHITE,DPHI,SPHI
      COMMON/C8/REO
      NQ=MINO(NP,15)
      DO 20 I=2,NQ
      NU=NP-I+1
      JR=MQB(NU)
      NJ=MBL(NU)+1
      DO 20 J=1,JR
      K=1+IABS(MP-J)
      DPHI=VPIC(K,I)
      IF (J.EQ.1) GO TO 10
      K=MP+J-1
      DPHI=DPHI+VPIC(K,I)
10  SPHI=SPHI+DPHI*DS(NJ)
20  NJ=NJ+1
      RETURN
      END
$      FORTRAN NLSTOU,DECK
CMSIMEC      MSIMEC
      FUNCTION MSIMEC(M,N,L,A,B)
      COMPLEX A,B,C
      DIMENSION AIM(1),B(M,1)
      DO 30 J = 1,N
      C = 0.0
      DO 10 J = 1,N
10  C=AMAX1(C,ABS(REAL(A(I,J))),ABS(AIMAG(A(I,J))))
      IF(C.EQ.0.0) GO TO 100
      DO 20 J = 1,N
20  A(I,J) = A(I,J)/C
      DO 30 J = 1,1
30  B(I,J) = B(I,J)/C
      IF(N.EQ.1) GO TO 205

```

```

NM = N - 1
DO 200 J = 1, NM
C = 0.0
K = 0
DO 40 I = J, N
D = ABS(REAL(A(I, J))) + ABS(AIMAG(A(I, J)))
IF (D .GE. D) GO TO 140
K = I
C = D
40 CONTINUE
IF (C .EQ. 0.0) C .LT. 1.E-7) GO TO 1000
IF (K .EQ. J) GO TO 70
DO 50 JJ = J, K
G = A(J, JJ)
A(J, JJ) = A(K, JJ)
50 A(K, JJ) = G
DO 60 JJ = 1, L
G = R(J, JJ)
R(J, JJ) = R(K, JJ)
60 R(K, JJ) = G
70 G = 1.0 / A(J, J)
JP = J + 1
DO 80 JJ = JP, N
80 A(J, JJ) = A(J, JJ) * G
90 DO 100 JJ = 1, L
100 R(J, JJ) = R(J, JJ) * G
DO 200 I = 1, N
IF (1.E0.J) GO TO 200
G = A(I, J)
DO 110 JJ = JP, N
110 A(I, JJ) = A(I, JJ) - G * A(J, JJ)
DO 120 JJ = 1, L
120 R(I, JJ) = R(I, JJ) - G * R(J, JJ)
200 CONTINUE
205 G = A(N, N)
IF (ABS(REAL(G)) + ABS(AIMAG(G)) .LT. 1.E-7) GO TO 1000
DO 210 J = 1, N
210 R(N, J) = R(N, J) / G
IF (C .EQ. 1) GO TO 230
DO 220 I = 1, NM
DO 220 JJ = 1, L
220 R(I, JJ) = R(I, JJ) - A(I, N) * R(N, JJ)
230 MSINEC = 1
RETURN
1000 MSINEC = 2
RETURN
END
*
C0C1J      F0PTRAN NLST00, D1 C1
          D01J
SUBROUTINE TQ1J
COMMON VPIF, DS, D, O, PHIW, CK, CZERO, PHI, PHIE, DPHI, SPHI
COMMON/C1/KOXY(2000), XF(5), YE(3), AR(3), X1, X2, X3, X4, Y1, Y2, BETA, NIS
COMMON/C3/C(10, 2, 2), NI(10, 2), NF(10, 2), NTMAX(2), FN(28), DXE(6), IP
COMMON/C4/VPIL(40, 15), DS(2000), DQ(28, 2), Q(10, 10, 3), PHIW(50), CK(40)
COMMON/C5/MOR(100), DPL(100), FQ, IFR, XL, NS, NIM, K, J, QR, QJ, QAB, QAN
COMMON/C6/X, Y, DX, DY, EM, EK, EKB, EKR, NP, MP, NB, KBOX, KODE, MODE, NBW, NBI
COMMON/C7/CZERO, P0I, PHIE, DPHI, SPHI
COMMON/C8/R00
DPHI = PHI * XF(5) / F
IF (NP .EQ. 1) DPHI = 0.5 * DPHI

```

SON/4950  
SON/4960  
SON/4970  
SON/4980  
SON/4990  
SON/5000  
SON/5010  
SON/5020  
SON/5030  
SON/5040  
SON/5050  
SON/5060  
SON/5070  
SON/5080  
SON/5090  
SON/5100  
SON/5110  
SON/5120  
SON/5130  
SON/5140  
SON/5150  
SON/5160  
SON/5170  
SON/5180  
SON/5190  
SON/5200  
SON/5210  
SON/5220  
SON/5230  
SON/5240  
SON/5250  
SON/5260  
SON/5270  
SON/5280  
SON/5290  
SON/5300  
SON/5310  
SON/5320  
SON/5330  
SON/5340  
SON/5350  
SON/5360  
SON/5370  
SON/5380  
SON/5390  
SON/5400  
SON/5410  
SON/5420  
SON/5440  
SON/5450  
SON/5460  
SON/5470  
SON/5480  
SON/5460  
SON/5500  
SON/5510  
SON/5520  
SON/5530  
SON/5540  
SON/5550

```

XP = X
IF(NS.EQ.2) XP = X - X3
PX = XP
K = 1
NIM = NIMAX(NS)
DO(1,NS) = DO(1,NS) + DPHI*CMPLX(0.0,-EK)
IF(NTH.EQ.1) GO TO 50
IF(XP.EQ.0.0) GO TO 30
YX = Y/XP
DO 20 N = 2,7
Z = PX
DO 10 M = 1,N
K = K + 1
IF(K.GT.NIM) GO TO 50
DOCK(NS) = DOCK(NS) + DPHI*Z*CMPLX(FN(K)/XP,-EK)
10 Z = Z*YX
20 PX = PX*XP
GO TO 50
30 PX = 1.0
DO 40 N = 2,7
K = K + N
KK = K - 1
IF(KK.LT.0) DOCK(K,NS) = DOCK(KK,NS) + DPHI*PX
PX = PX*Y
IF(K.GT.NIM) GO TO 50
40 DOCK(K,NS) = DOCK(K,NS) + DPHI*CMPLX(0.0,-EK*PX)
50 IF(MODE.NE.3) GO TO 90
DPHI = DPHI/DOCK(K,NS)
K = 1
YX = Y/XP
PX = 1.0/PX
DO 70 N = 1,7
Z = PX
DO 60 M = 1,N
DOCK(M,NS) = DOCK(M,NS) - DPHI*Z
K = K + 1
IF(K.GT.NIM) GO TO 80
60 Z = Z*YX
70 PX = PX*XP
80 ARG = EK*(X3 - X1)
DPHI = -DPHI*CMPLX(COS(ARG),-SIN(ARG))
X1 = 0.0
CALL QEGF
90 IF(MODE.NE.5) RETURN
X4 = X4
IF(MP.EQ.1) PHIDF = 0.5*PHIDE
DPHI = PHIDF
CALL QEGF
RETURN
END

```

\$ IFORTAN INLSROU,DECK  
 QEGF

SUBROUTINE QEGF

COMPLEX WPIC,DS(40),PHIWK,CZERO,PHI,PHIDE,DPHI,SPHI

COMMON/C4/WPIC(40),DS(2000),DO(28,2),Q(40,10,3),PHIW(50),CK(40)

COMMON/C5/M(100),NBL(100),FIO,IFR,XL,NS,NIM,K,J,QR,WI,QAB,QAN

COMMON/C6/X,Y,IX,IY,IEK,ENB,ENR,NP,IP,NB,KROX,KODE,MODE,NBW,NBT

COMMON/C7/CZERO,PHI,PHIDE,DPHI,SPHI

COMMON/C8/IRIP

IPX=1.07PX

SON75560  
 SON75570  
 SON75580  
 SON75590  
 SON75600  
 SON75610  
 SON75620  
 SON75630  
 SON75640  
 SON75650  
 SON75660  
 SON75670  
 SON75680  
 SON75690  
 SON75700  
 SON75710  
 SON75720  
 SON75730  
 SON75740  
 SON75750  
 SON75760  
 SON75770  
 SON75780  
 SON75790  
 SON75800  
 SON75810  
 SON75820  
 SON75830  
 SON75840  
 SON75850  
 SON75860  
 SON75870  
 SON75880  
 SON75890  
 SON75900  
 SON75910  
 SON75920  
 SON75930  
 SON75940  
 SON75950  
 SON75960  
 SON75970  
 SON75980  
 SON75990  
 SON76000  
 SON76010  
 SON76020  
 SON76030  
 SON76040  
 SON76050  
 SON76060  
 SON76080  
 SON76090  
 SON76100  
 SON76110  
 SON76120  
 SON76130  
 SON76140  
 SON76150  
 SON76160

```

IF(XL.F0.0.0) GO TO 30
YX=Y/XL
K=1
DO 20 N=1,7
PY=FX
DO 10 M=1,N
DO(K,2) = DO(K,2) - DPHI*PY
IF(K.EQ.NTM) RETURN
K=K+1
10 PY=PY*YX
20 PX=PX*XL
RETURN
30 K = 0
DO 40 N = 1,7
K = K + N
IF(K.GT.NTM) RETURN
DO(K,2) = DO(K,2) - DPHI*PX
40 PX = PX*Y
RETURN
END
4  LOPTRAN NISTAD, DPHI
CPCT  .PHI
SUBROUTINE FOUT(IID)
COMPLEX VPID,DS,DQ,Q,PHIW,CK,CZERO,PHI,PHITE,DPHI,SPHI
DIMENSION S(4,3),SURF(2,3),CON(7),C(50)
DIMENSION CAPS(2,50)
COMMON/C1/K,DX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BE1A,NBS
COMMON/C2/AS,MAC,BFMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LESSVPS
COMMON/C3/CD(10,26,2),NI(10,2),NF(10,2),NTMAX(2),FN(28),DXE(6),TP
COMMON/C4/VLIC(80,15),DS(2000),DQ(26,2),Q(10,10,3),PHIW(50),CK(40)
COMMON/C5/HOB(100),NRL(100),FO,IFR,XL,NS,NTM,K,J,QR,QI,QAB,QAN
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,RP,NB,NBOX,KUDE,MODE,NBW,NBT
COMMON/C7/CZERO,PHI,PHITE,DPHI,SPHI
COMMON/C8/R00
DATA (SW(1,1),I=1,6)/26HMAP OF SONIC BOX OVERLAY ,
1 26HON WING, TAIL AND WAKE ,
2 26H (S) - WING ,
3 26H (S) - TAIL ,
4 26H (,) - WAKE ,
5 26H /
DATA (SURF(1,1),I=1,3)/8HWING ,8HTAIL ,11HWING + TAIL /
DATA CON/1HS,1HT,1HS,1HX,1HS,1H,,1H./
GO TO (10,20,30,40,50,60,70,80),IND
10 WRITE(6,11) EM,AS,PHI,XE(1),XE(4),X1,X4,Y1,Y2,Y2,X2,X4,
IAR(1),AR(2),NBW,NBT,NBS,NBS
11 FORMAT(1H1/////////3,X,43HHAC/NAA MISSILE TRANSONIC AIRLOADS PROGRAM
1 ///37X,30HIGHLIGHT CONDITIONS AND GEOMETRY/1H0//15X, 13HMACH NUMBERS
2 =,18.5,4X,16HSPED OF SOUND =F10.3,4H L/T,4X,4HRHO=,E14.8//1H0/
X54X,4HWING,1HX,
3 4HTAIL//22X,15H1.1. STATION (L),2F22.3//22X,16HROOT CHORD (L),
4 2F22.3// 22X,15H1.1. SPAN (L),2F22.3//22X,16HT.E. SPAN (L),
5 2F22.3// 22X,15H1.1. CHORD (L),2F22.3//22X,16HTOTAL AREA (L*L),
6 2F22.3// 22X,15HCHORDWISE BOXES ,119,122//
7 22X,16HSPANWISE BOXES ,119,122)
WRITE(6,12) BOX,DX,DY
12 FORMAT(1H0//,11X,25HCHORDWISE BOXES =,13, 5X,11HBOX CHORD =,
1 1P1F12.5,2H1, 5X,10HBOX SPAN =,1P1F12.5,2H L/ )
WRITE(6,91)
NB = 1
DO 17 NP = 1,4RDX

```

PB = HOB(NP)	SON76770
DO 13 MP = 1, MB	SON76780
K = KROX(NP)	SON76790
C(MP) = COD(K)	SON76800
13 NB = NB + 1	SON76810
IF(NP.GT.6) GO TO 15	SON76820
WRITE(6,14) (SH(I,MP), I=1,5), (C(MP), MP=1, MB)	SON76830
14 FORMAT(10X, 5A6, 50A1)	SON76840
GO TO 17	SON76850
15 WRITE(6,16) (C(MP), MP=1, MB)	SON76860
16 FORMAT(40X, 50A1)	SON76870
17 CONTINUE	SON76880
GO TO 1000	SON76890
20 WRITE(6,51) FREQ(IFR), NBOX, EKR, EM	SON76900
WRITE(6,21) CM, EKR	SON76910
21 FORMAT(1H, 28X, 48HPIANAR VELOCITY POTENTIAL INFLUENCE COEFFICIENTSSON76920	
1 /1H0, 30X, 1H MACH NO. =, F8.5, 10X, 6HKBAR =, F9.5/1H0, 13X, 1H1, 5X, 1HJSON76930	
2 10X, 5HNUBAR, 5X, 5H MUBAR, 11X, 14HREAL VPIC(J, I), 8X, 14HIMAG VPIC(J, I)SON76940	
3 /1H )	SON76950
JBOX = 2*HOB(NBOX)-1	SON76960
IBOX = MIN0(NBOX, 15)	SON76970
DO 22 I = 1, IB0X	SON76980
DO 22 J = 1, JBOX	SON76990
BAP00 = J - 1	SON77000
BAP01 = J - 1	SON77010
22 WRITE(6,23) I, J, BAP00, BAP01, VPIC(J, I)	SON77020
23 FORMAT(9X, 216, 4X, 2F10.1, 2X, 1P2E22.5)	SON77030
GO TO 1000	SON77040
30 WRITE(6,51) FREQ(IFR), NBOX, EKR, EM	SON77050
WRITE(6,51) CM, EKR	SON77060
31 FORMAT(1H, 21X, 59HUPPER VELOCITY POTENTIALS AND SURFACE UPWASHES FSON77070	
(OR MODE NO., 13/ 1H0, 9X, 1HN, 6X, 1HM, 5X, 2HNB, 7X, 10HR PHI(N, M), 7X, 10HISON77080	
2 PHI(N, M), 10X, 9HR W(N, M), 8X, 9HI W(N, M)/1H )	SON77090
GO TO 1000	SON77100
40 SPH1 = DS(NH)/E1	SON77110
WRITE(6,41) MP, MB, NB, SPH1, CK(MP)	SON77120
41 FORMAT(4X, 317, 1P2E17.5, 3X, 1P2E17.5)	SON77130
GO TO 1000	SON77140
60 IF(NS.EQ.3) GO TO 100	SON77150
50 WRITE(6,51) FREQ(IFR), NBOX, EKR, EM	SON77160
51 FORMAT(1H1, 33X, 43HMISSILE TRANSONIC AIRLOADS PROGRAM (CONT-D))//1H0SON77170	
1 8X, 27HOSCILLATORY FREQUENCY (CPS), F12.5, 14X, 12, 25H BOXES IN CHORDSON77180	
2 DIRECTION /1H0, 8X, 30HREDUCED FREQUENCY (SEMI CHORD), F9.5, 14X, SON77190	
3 23HFREE STREAM MACH NUMBER, F9.3, /1H )	SON77200
WRITE(6,101) SURF(1, NS)	SON77210
101 FORMAT(28X, 45HINPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR , A6/ SON77220	
1 22X, 62HREFERENCE TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECSON77230	
2 ION //2X, 4HMODE, 20X, 7HCUEFFS.)	SON77240
DO 102 I=1, NMODE	SON77250
NIM=NT(1, NS)	SON77260
102 WRITE(6,103) I, (CO(1, J, NS), J=1, NIM)	SON77270
103 FORMAT(1H0, 14, 4X, 1P7E13.4/(9X, 1P7E13.4))	SON77280
100 WRITE(6,51) FREQ(IFR), NBOX, EKR, EM	SON77290
WRITE(6,61) (SURF(1, NS), I=1, 2)	SON77300
61 FORMAT(1H, 35X, 23HGENERALIZED FORCES FOR , 2A6/1H0, 6X, 4HDEFL, 3X, SON77310	
1 4HLOAD, 10X, 9HREAL PART, 10X, 9HIMAG PART, 10X, 9HAUS VALUE, 10X, SON77320	
2 11HPHASE ANGLE /1H )	SON77330
GO TO 1000	SON77340
70 WRITE(6,71) J, K, JR, Q1, QAH, QAN	SON77350
KKK=2*NMODE	*****

NNN=2*K	*****
NNNN=NNN-1	*****
CARDS(J,NNN)=QR	*****
CARDS(J,NNN)=01	*****
IF (NSURF .EQ. 1) GO TO 667	
IF (NS.NE.3) GO TO 1000	*****
667 IF (J.NE.NMODE) GO TO 1000	*****
IF (K.NE.NMODE) GO TO 1000	*****
KKK=2*NMODE	*****
PUNCH 666, ((CARDS(II,JJ),JJ=1,KKK),II=1,NMODE)	*****
666 FORMAT(6E12.5)	*****
71 FORMAT(1H0,19,17,2X,1P3E19.5,0PF16.3,4H DEG)	SON77380
GO TO 1000	SON77370
80 WRITE(6,91)	SON77380
WRITE(6,81) FREJ(1FR)	SON77390
81 FORMAT(1H0////////24X,56HUNABLE TO OBTAIN COMPLEX SIMULTANEOUS EQUATIONS SOLUTION//31X,42HCOMPUTATIONS FOR THIS FREQUENCY TERMINATED,2/45X, 6HFRE. =,19.3)	SON77400
91 FORMAT(1H1,30X,13HMISSILE TRANSONIC AIRLOADS PROGRAM (CONT-D)//)	SON77410
1000 RETURN	SON77420
END	SON77430
	SON77440
	SON77450



## 5.0 SUPERSONIC UNSTEADY AERODYNAMICS

### 5.1 Theoretical Derivation

For Mach numbers greater than 1.0, the linearized flow equation becomes a hyperbolic differential equation:

$$(M^2 - 1) \phi_{xx} - \phi_{yy} - \phi_{zz} = -M^2 \left[ 2ik \phi_x - k^2 \phi \right] \quad (5.1.1)$$

The equation only has solutions within characteristic regions called Mach cones. Linearized supersonic flow theory has led to closed-form solutions for many types of lifting surfaces in steady flow. These solutions are easily derived because the influence of a small perturbation is confined to its downstream or aft Mach cone. Conversely, the only disturbances that can influence a particular point are confined to its upstream or fore Mach cone.

Equation (5.1.1) is satisfied by a pulsating source. The source, placed at  $(\xi, \eta, \zeta)$ , emanates spherical disturbances and has a velocity potential induced at  $(x, y, z)$  given by

$$\phi_s = A(\xi, \eta, \zeta) G(x - \xi, y - \eta, z - \zeta) \quad (5.1.2)$$

where

$$G(x - \xi, y - \eta, z - \zeta) = -\frac{1}{\pi R} \exp[-ik(x - \xi)] \cos\left[\frac{\bar{k}}{M} R\right] \quad (5.1.3)$$

$$R = \sqrt{(x - \xi)^2 - (M^2 - 1)[(y - \eta)^2 + (z - \zeta)^2]} \quad (5.1.4)$$

$$\bar{k} = k M^2 / (M^2 - 1) \quad (5.1.5)$$

and  $A(\xi, \eta, \zeta)$  = source strength

This type of disturbance has no influence outside the downstream Mach cone and is discontinuous at the point  $(\xi, \eta, \zeta)$ . To provide the necessary antisymmetry of disturbances associated with lifting surfaces, we place a pair of sources on either side of the  $z = 0$  plane and require the lower source strength to be equal in magnitude but opposite in sense to the upper source strength.

Applying this source superposition technique to the wing, wake and control surface, the entire  $z = 0$  plane is covered above and below with source sheets. The strength of the opposing sheets are equal in magnitude but opposite in sense;  $A(\xi, \eta, 0^+) = -A(\xi, \eta, 0^-)$ . The strength distribution has been shown by Garrick and Rubinow (Reference 8) to be equal everywhere to the local downwash. Using this condition, we have

$$A(\xi, \eta, 0^+) = w(\xi, \eta, 0^+) \quad (5.1.6)$$

The velocity potential at  $(x, y, 0^+)$  can be written as

$$\phi = \iint w(\xi, \eta) G(x - \xi, y - \eta) d\xi d\eta \quad (5.1.7)$$

The range of integration extends over the region contained in the fore Mach cone of the point.

In the wake region between the wing and control surface, the downwash must be determined to satisfy the continuous pressure condition. This is the same relationship given by Equation (4.1.7) in the transonic unsteady aerodynamics discussion. Substituting Equation (5.1.7) in the wake condition gives

$$\iint w(\xi, \eta) G(x - \xi, y - \eta) d\xi d\eta = \phi_{\text{wing t.e.}} \left[ \exp -ik(x - x_{\text{wing t.e.}}) \right] \quad (5.1.8)$$

This relationship which requires knowledge of the upstream downwash within the fore Mach cone to solve for the local downwash.

The preceding discussion applies only to lifting surfaces with supersonic leading edges. When the leading edges are supersonic, the fluid flow over the top and bottom of the lifting surfaces are completely isolated from one another. To treat the problem of subsonic leading edges, the concept of a diaphragm of unknown downwash is added to the planform. The diaphragm region is between the Mach envelope and subsonic edge. The diaphragm downwash is found by applying the condition of zero pressure:

$$0 = \iint w(\xi, \eta) G(x - \xi, y - \eta) d\xi d\eta \quad (5.1.9)$$

The downwash of the diaphragm creates an additional contribution to the pressure profile over the planform.

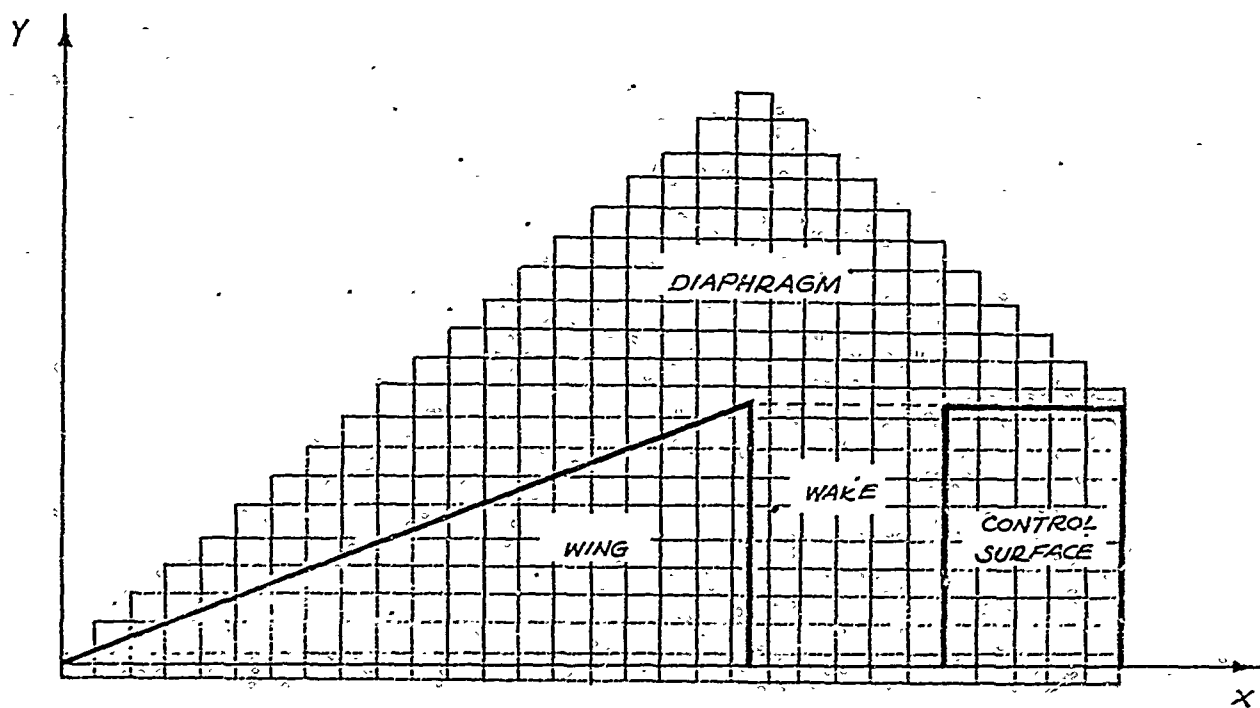


Figure 5.1.1 Mach Box Overlay Pattern

The velocity potential distribution is found by the so called Mach box method. The wing, control surface, wake and diaphragm regions are covered with a grid of rectangular boxes of length  $\Delta$ . The width of the boxes is set equal to  $\Delta / \sqrt{M^2 - 1}$  thus making the box diagonals parallel to the Mach lines. The source strength (downwash) is assumed constant over each box and equal to the value at the box center. A typical Mach box overlay is shown in Figure (5.1.1).

From the conditions imposed on the planform, the downwash can be numerically evaluated for the diaphragm and wake boxes and the velocity potential profile can be established for any deformation mode. The pressure can then be calculated from Equation 4.1.8 and generalized forces can be evaluated with Equation 2.0.1.

## 5.2 PROGRAM DESCRIPTION

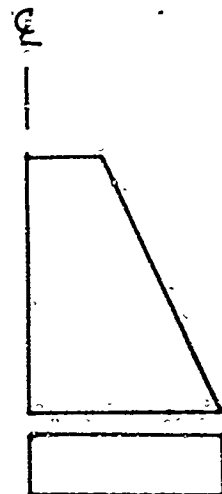
The Supersonic Unsteady Aerodynamics Program calculates generalized forces for up to 10 deformation modes. The computer solution is based upon the Mach box technique. The various configurations which can be analyzed are shown in Figure 5.2.1 and Table 5.2.1. The analysis includes interaction effect between tandem surfaces and wake effects on the trailing surface. Single surfaces may be analyzed by inputting a second surface with a zero chordlength.

The supersonic Mach box method uses source superposition method to approximate the aerodynamic forces on an oscillating thin planar surface. The diaphragm concept was employed to handle subsonic leading edges and gaps between the aerodynamic surfaces. For purposes of calculating pressures, it was assumed that the source strength over the area of each box is a constant value which satisfies the condition of tangential flow at the center of the box. The Mach box procedure is basically the same as the method of Pines, et al, Reference II, differing only in that the surface and diaphragm is overlaid with a grid of rectangular boxes, the diagonals of which are parallel to Mach lines. As in the subsonic and transonic cases, the potential equation is written as an integral equation (this time relating the downwash to the source strengths) and approximated by a matrix equation. The numerical difficulties are primarily ones of computer logic since the zones of influence of a given Mach box is limited to the region within the aft Mach lines. The matrix formulation leads to a partitioned form since there are two boundary conditions to be matched. The first boundary condition is the downwash on the surface, and the second is that there be no pressure difference off of the surface in the diaphragm regions. The zero pressure conditions leads to a relationship between the diaphragm potentials and the surface potentials, and the surface downwash condition then leads to the surface potentials. The surface pressures then follow from the surface potentials.

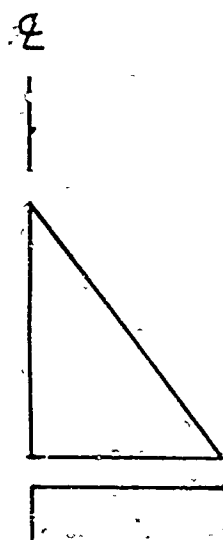
The solution for the generalized aerodynamic forces requires the input of the deformation modes due to vibration. The program considers the modes to be expressed as analytic functions of the form:

$$w(x, y) = \sum_{m=0}^N \sum_{n=0}^n c_{(n-m), m} x^{(n-m)} y^m$$

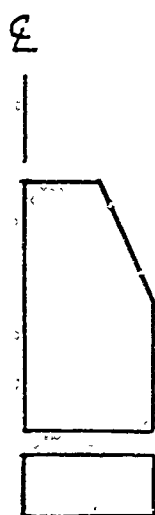
To meet this requirement only the coefficients "c" are required as input into the program. These coefficients can be obtained in several ways, the most common way is to surface fit the modes by the least-square technique.



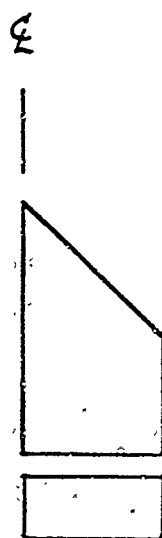
TRAPEZOIDAL



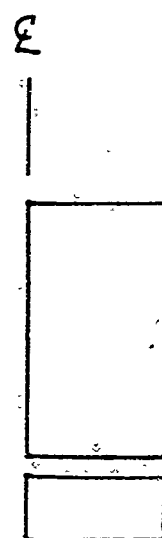
DELTA



TRAPEZOIDAL  
(CROPPED)



DELTA  
(CROPPED)



RECTANGULAR

FIGURE 5.2.1  
TANDEM COPLANAR CONFIGURATIONS AT SUPERSONIC  
MACH NUMBER

TABLE 5.2.1- OPTIONAL CONFIGURATIONS

CONFIGURATION	CHORDWISE COORDINATE	SPANWISE COORDINATE
RECTANGULAR	$X(1) \neq 0.0$ $X(2) = 0.0$ $X(3) > 0.0$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
DELTA	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > 0.0$
TRAPEZOIDAL	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) = X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
TRAPEZOIDAL (CROPPED)	$X(1) = 0.0$ $X(2) > X(1)$ $X(3) > X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) > 0.0$ $Y(3) > Y(2)$
DELTA (CROPPED)	$X(1) = 0.0$ $X(2) > 0.0$ $X(3) > X(2)$ $X(4) \geq X(3)$ $X(5) \geq X(4)$	$Y(1) = 0.0$ $Y(2) = 0.0$ $Y(3) > Y(2)$

### 5.3 INPUT INSTRUCTIONS

Instructions for preparing input data for the supersonic computer program are presented here. The field location and format for each quantity is specified. Any set of units may be used for geometric dimensions and acoustic velocity as long as they are consistent, e.g., if inches is used for length, then the acoustic velocity must have dimensions of inches per second. The required data and the sequence in which the information is entered is as follows:

#### 1. Streamwise Coordinates (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	X(1)	X(2)	X(3)	X(4)	X(5)	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) X(1) Wing root leading edge coordinate (see Figure 5.3.1)
- (2) X(2) Wing tip leading edge coordinate
- (3) X(3) Wing trailing edge coordinate
- (4) X(4) Control surface leading edge coordinate
- (5) X(5) Control surface trailing edge coordinate

A single surface, the wing, may be analyzed by setting X(4) and X(5) equal to X(3). The various configurations are generated as shown in Table 5.2.1. The origin for the planform and AIC station coordinates must be at the leading edge root of the wing, therefore X(1) and Y(1) described below, must always be zero.

#### 2. Spanwise Coordinates and Acoustic Velocity (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	Y(1)	Y(2)	Y(3)	SOUND	RHØ	
Item	(1)	(2)	(3)	(4)	(5)	

- (1) Y(1) Wing root spanwise coordinate
- (2) Y(2) Wing leading edge spanwise coordinate
- (3) Y(3) Wing (and control surface) tip spanwise coordinate
- (4) SOUND Speed of sound at altitude for which analysis is performed
- (5) RHØ Density of fluid \* 1000.0 (M./L<sup>3</sup>)



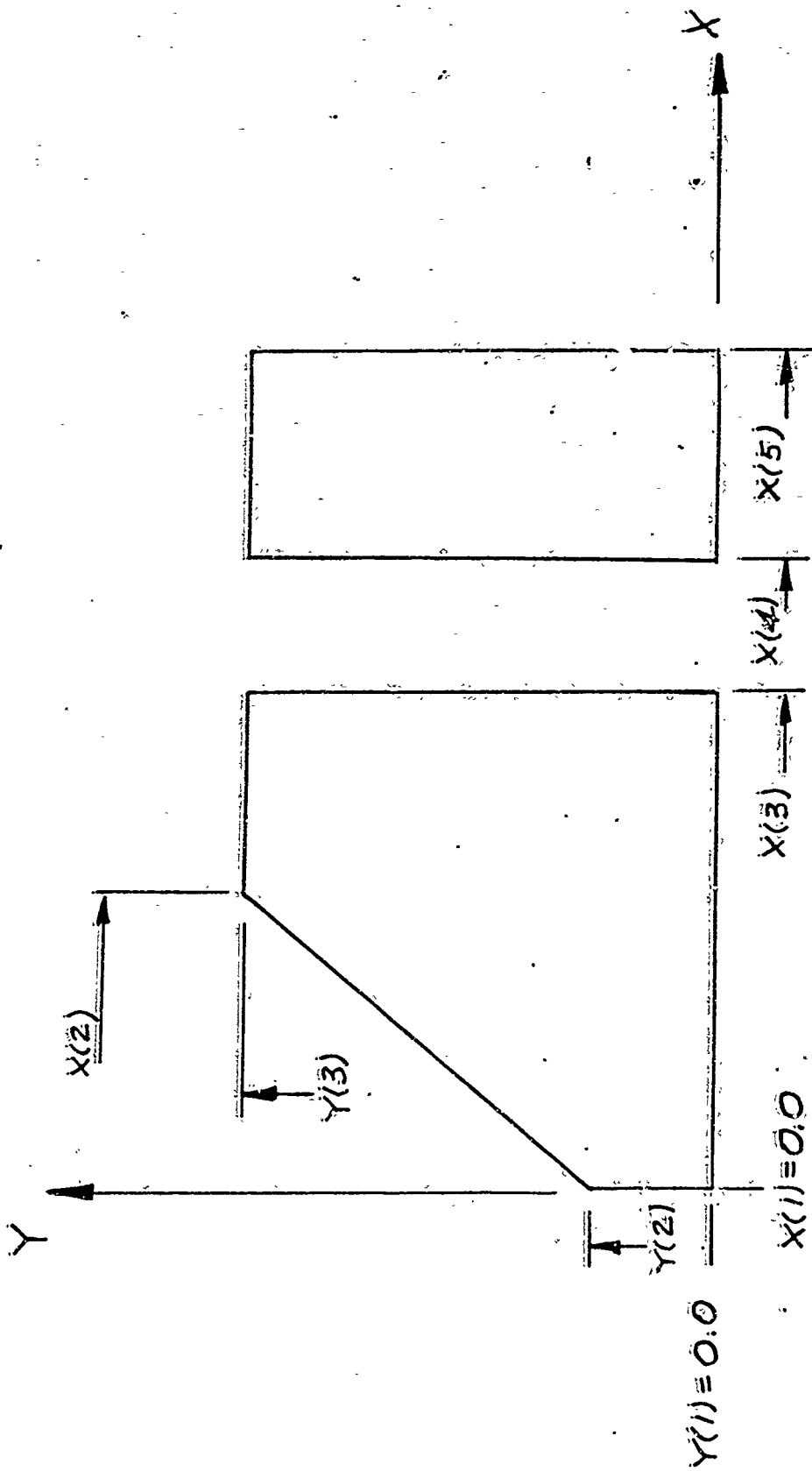


FIGURE 5.3.1  
GEOMETRY DESCRIPTION

### 3. General Information (6I12 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NMACH	NFREQ	NMODES	NBW	LVPIC	LSSVP
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) NMACH Number of Mach numbers (max 6)  
 (2) NFREQ Number of input frequencies (max 10)  
 (3) NMODES Number of input modes (max 10)  
 (4) NBW Number of chordwise wing boxes (max 10)  
 (5) LVPIC Print velocity potential influence coefficients; 0 ~ No, 1 ~ Yes  
 (6) LSSVP Print upwashes; 0 ~ No, 1 ~ Yes

### 4. Mach Numbers (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FMACH(1)	FMACH(2)	FMACH(3)	FMACH(4)	FMACH(5)	FMACH(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) FMACH(i) Mach numbers for which the analysis is to be performed.

### 5. Frequency (6E12.5 format)

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	FREQ(1)	FREQ(2)	FREQ(3)	FREQ(4)	FREQ(5)	FREQ(6)
Item						

- (1) FREQ Frequencies for which the analysis is to be performed.  
 Continue on next card for FREQ(i) > 6

### 6. Deformation Modes. Repeat the following Cards NMODES Times

(6I12) Format.						
Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM1(i)	NFI				
Item	(1)	(2)				

- (1) NTM1(i) Number of deformation mode coefficients for the wing, mode i  
 (2) NFI Compute generalize forces; 0 ~ No, 1 ~ Yes  
 If NFI = 0, the program will compute the VPIC's and stop.

## (6E12.5) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	CØ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- (1) CØ(i)  $i = 1$ , NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; where the first integer is the power of  $x$  and the second is the power of  $y$ . Continue on successive card until all polynomial coefficients are input.

## (6I12) Format

Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	NTM(i)	NFI				
Item	(1)	(2)				

- (1) NTM2(i) Number of deformation mode coefficients for the control surface, mode (i)
- (2) NFI Compute generalized forces; 0 ~ No; 1 ~ Yes. If NFI = 0, the program will compute the VPIC's and stop.

## (6E12/5) Format

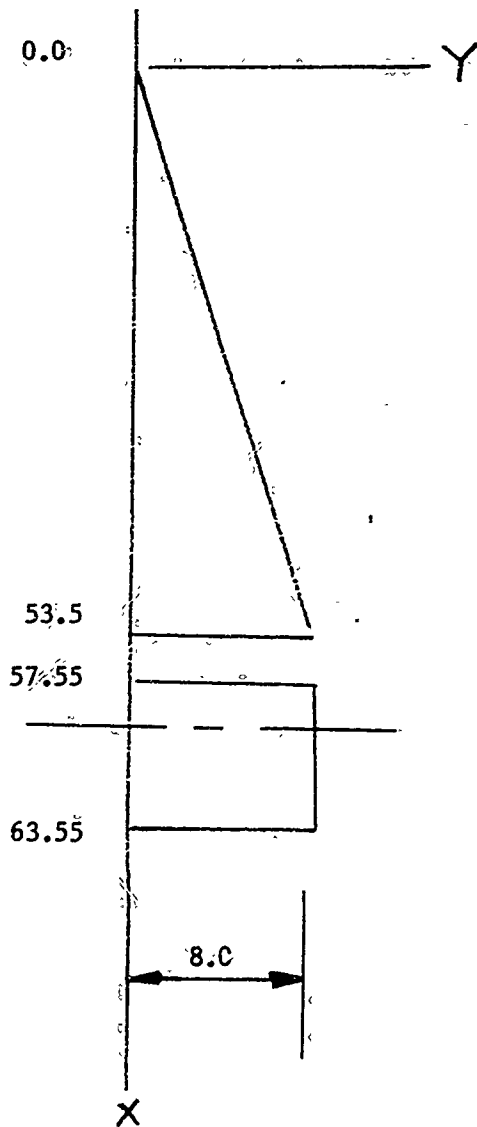
Column	1-12	13-24	25-36	37-48	49-60	61-72
Name	CØ(1)	CØ(2)	CØ(3)	CØ(4)	CØ(5)	CØ(6)
Item	(1)	(2)	(3)	(4)	(5)	(6)

- CØ(i)  $i = 1$ , NTM deformation polynomial coefficients to be input in the following order: 0,0; 1,0; 0,1; 2,0; 1,1; 0,2; 3,0; etc. where the first integer is the power of " $x$ " and the second is the power of " $y$ ". Continue on successive cards until all polynomial coefficients are input.

#### 5.4 SAMPLE PROBLEM

The generalized forces are calculated for the configuration below. The flight parameters and pertinent input data are on the first page of the computer print out.

The coefficients of the deformation modes for the forward surface are shown on the third page of the computer print out, and for the aft surface on the fifth page of the computer print out.



# HAC/NAA MISSILE SUPERSONIC AIRLOADS PROGRAM

## FLIGHT CONDITIONS AND GEOMETRY

MACH NUMBER = 1.50900      SPEED OF SOUND = 13392.000 L/T       $RHO = 0.11460000E-06$

	WING	TAIL
L.E. STATION (L)	0.	57.550
ROOT CHORD (L)	53.500	6.000
L.E. SPAN (L)	0.	8.000
T.E. SPAN (L)	8.000	8.000
TIP CHORD (L)	0.	6.000
TOTAL AREA (L*L)	428.000	96.000
CHORDWISE BOXES	40	4
SPANWISE BOXES	7	7

TOTAL CHORDWISE BOXES = 47      BOX CHORD = 1.35443E 00 L      BOX SPAN = 1.21144E 00 L

(S) - WING  
 (S) - TAIL  
 (.) - WAKE  
 (.) - DIAPHRAGM

# MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR WING  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE	COEFS.						
1	-2.7643E-03	-2.3968E-03	1.0698E-01	3.3227E-04	-1.7350E-02	-3.6455E-02	-2.0567E-05
	1.0242E-03	-1.5649E-03	2.5596E-02	5.4159E-07	-2.8225E-05	2.0969E-04	-1.7662E-03
	1.4567E-03	-4.8146E-09	2.6893E-07	-3.0507E-06	2.2374E-05	-1.5766E-05	-2.0292E-05
2	5.9081E-04	1.1346E-02	-1.4269E-01	-1.9870E-03	1.7391E-02	-5.2818E-02	1.2097E-04
	-2.0628E-03	3.7740E-02	-1.1759E-01	-2.9744E-06	7.7451E-05	-1.5215E-03	4.6965E-03
	1.1664E-03	2.4952E-08	-8.3941E-07	1.6896E-05	-7.6407E-05	2.3531E-04	-7.3812E-04
3	1.6687E-02	-1.9542E-02	-1.5043E 00	3.1005E-03	2.2035E-01	1.6944E-01	-1.9229E-04
	-9.0043E-03	-2.6816E-02	8.1504E-02	4.8204E-06	1.3340E-04	9.4618E-04	-2.3806E-03
	-7.3799E-03	-4.0844E-08	-5.5376E-07	-1.4601E-05	1.3599E-04	-9.1914E-04	3.1280E-03
4	1.3375E-01	-9.8015E-03	1.4319E 00	3.0046E-03	-3.8145E-01	6.0607E-01	-2.9098E-04
	2.8713E-02	-1.2993E-01	3.2289E-01	9.6282E-06	-8.5727E-04	6.9968E-03	-3.3429E-02
	5.4256E-02	-9.6391E-08	8.2378E-06	-8.4006E-05	3.9512E-04	-1.0736E-04	-2.7726E-03
5	-2.3479E-04	-5.1973E-03	2.3344E-01	3.7865E-04	-3.3701E-04	-2.7195E-01	-6.4710E-06
	-8.1025E-04	1.3782E-02	5.7945E-02	-4.9236E-08	2.7581E-05	-2.6211E-04	-1.5177E-03
	-5.9560E-03	1.3471E-09	-2.6464E-07	2.2137E-06	-1.5090E-08	1.5586E-04	-1.3277E-04

# MISSILE SUPERSONIC AIRLANS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

## GENERALIZED FORCES FOR WING

DEFL	LOAD	REAL PART	IMAG PART	ANS VALUE	PHASE ANGLE
1	1	-4.05330E-01	1.41647E-01	4.29367E-01	160.737 DEG
1	2	2.48826E 00	-2.46939E 00	3.50561E 00	-44.762 DEG
1	3	5.69256E 00	2.42253E-01	5.69771E 00	2.437 DEG
1	4	-6.52883E 00	-1.33247E 00	6.66342E 00	-168.465 DEG
1	5	3.05956E-01	-5.45114E-02	3.09994E-01	-8.472 DEG
2	1	5.42497E 00	1.01807E-01	5.42594E 00	1.075 DEG
2	2	-1.13634E 02	5.50276E 01	1.26256E 02	154.161 DEG
2	3	-1.17337E 02	-9.03881E 01	1.48114E 02	-142.392 DEG
2	4	3.85767E 01	7.90880E 01	8.79948E 01	63.998 DEG
2	5	-1.54986E 01	1.65535E 00	1.55866E 01	173.984 DEG
3	1	-3.47591E 00	-4.56201E 00	5.73532E 00	-127.385 DEG
3	2	4.30375E 01	5.02509E 01	6.61678E 01	49.426 DEG
3	3	5.43115E 01	1.55744E 02	1.64942E 02	70.775 DEG
3	4	-8.58316E 01	-6.56561E 01	1.08064E 02	-142.586 DEG
3	5	2.34054E 01	9.49312E 00	2.52574E 01	22.877 DEG
4	1	3.10905E-01	4.44125E 00	1.45212E 00	85.996 DEG
4	2	-6.41152E 01	-8.88772E 00	6.47282E 01	-172.188 DEG
4	3	-4.63360E 01	-1.24207E 02	1.32569E 02	-118.458 DEG
4	4	-3.63002E 01	8.41059E 01	9.16852E 01	113.345 DEG
4	5	-1.47609E 01	-2.25630E 00	1.49333E 01	-171.389 DEG
5	1	-1.45288E-01	-5.12284E-02	1.54055E-01	-168.577 DEG
5	2	-8.22063E 00	7.77921E 00	1.13179E 01	136.580 DEG
5	3	2.71663E 00	1.56198E 00	3.13366E 00	29.898 DEG
5	4	-1.62163E 01	3.83596E 00	1.66638E 01	166.691 DEG
5	5	8.47165E-01	1.39315E 00	1.63051E 00	58.697 DEG



# MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

INPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR TAIL  
 REFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECTION

MODE

COEFFS.

1	-2.9509E-01 -1.4897E-03 1.5973E-04	4.3922E-02 5.5863E-03 -6.5762E-02 -6.6256E-04	-7.3360E-03 -5.0795E-04	-2.6048E-03 3.6026E-04	-8.2124E-03 -2.1683E-04	3.9367E-03 -4.8161E-04
2	-5.2445E-03 -1.8634E-04 -9.1426E-05	-1.8889E-02 -6.7727E-04 -1.4280E-03 1.2652E-03	9.7705E-03 2.2149E-04	5.1856E-04 4.6749E-05	-5.6169E-03 -9.4713E-06	-2.6629E-03 6.8936E-05
3	3.6644E-02 -2.6833E-04 -1.2438E-05	-2.5725E-02 -7.2607E-04 -9.3449E-03 1.7027E-04	5.2614E-03 1.3103E-04	3.2757E-03 -1.3270E-05	-3.2647E-05 5.1347E-05	-1.4688E-03 2.3310E-05
4	-9.8849E-02 2.5576E-03 -1.2428E-04	-6.4342E-03 -8.0436E-03 4.6537E-02 1.7425E-03	8.2901E-04 2.8345E-04	1.8417E-02 -1.8412E-04	3.7439E-04 -9.9538E-05	-2.0627E-03 6.3188E-04
5	-5.7341E-01 -2.9503E-03 -6.1575E-05	3.1192E-01 -2.7418E-03 -9.6235E-03 8.1679E-04	-5.6429E-02 -1.2591E-03	2.0184E-02 1.8190E-04	-2.2471E-03 1.6698E-04	1.4691E-02 1.7044E-04

# MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (CPS) 200.00000 4/ BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

## GENERALIZED FORCES FOR TAIL

DEFL.	LOAD	REAL PART	IMAG PART	AUS VALUE	PHASE ANGLE
1	1	-2.38915E 02	1.28104E 02	2.71095E 02	151.000 DEG
1	2	3.49540E 01	8.58631E 01	9.27237E 01	67.054 DEG
1	3	-7.81320E 01	-1.35909E 01	7.93060E 01	-170.132 DEG
1	4	1.81209E 02	-3.54137E 01	1.84637E 02	-11.058 DEG
1	5	-9.35040E 02	9.55015E 01	9.39905E 02	174.168 DEG
2	1	-3.06021E 01	1.54906E 01	3.43021E 01	153.143 DEG
2	2	4.00729E 00	1.35986E 01	1.41767E 01	73.503 DEG
2	3	-1.60314E 01	6.41368E-01	1.60445E 01	177.709 DEG
2	4	3.01083E 01	-6.17353E 00	3.07347E 01	-11.508 DEG
2	5	-1.24952E 02	7.03793E 00	1.25155E 02	176.776 DEG
3	1	-1.43359E 01	7.51749E 00	1.61874E 01	152.328 DEG
3	2	1.61241E 00	7.73430E 00	7.90059E 00	78.224 DEG
3	3	-1.05254E 01	1.96083E 00	1.07064E 01	169.447 DEG
3	4	1.81686E 01	-4.84012E 00	1.88022E 01	-14.917 DEG
3	5	-6.27252E 01	1.56343E 00	6.27447E 01	170.572 DEG
4	1	7.90217E 01	-3.60158E 01	8.68422E 01	-24.582 DEG
4	2	-1.19493E 01	-2.54166E 01	2.80859E 01	-115.100 DEG
4	3	4.69554E 01	5.26476E 00	4.72496E 01	6.397 DEG
4	4	-8.27282E 01	2.59885E 00	8.67142E 01	162.560 DEG
4	5	2.76223E 02	-8.07811E 00	2.76342E 02	-1.675 DEG
5	1	-1.26964E 01	3.08803E 00	1.38620E 01	166.413 DEG
5	2	5.47163E 00	-2.04463E 01	2.11955E 01	-75.018 DEG
5	3	5.91118E 01	-2.80330E 01	6.54221E 01	-25.372 DEG
5	4	-6.53213E 01	2.68424E 01	7.86214E 01	157.661 DEG
5	5	1.87717E 01	3.74297E 01	4.18731E 01	63.365 DEG

# MISSILE SUPERSONIC AIRLOADS PROGRAM (CONT'D)

OSCILLATORY FREQUENCY (GPM) 200.00000 47 BOXES IN CHORD DIRECTION  
 REDUCED FREQUENCY (SEMI CHORD) 1.67339 FREE STREAM MACH NUMBER 1.500

## GENERALIZED FORCES FOR WING + TAIL

DEFL. LOAD	REAL PART	IMAG PART	ABS VALUE	PHASE ANGLE
1 1	-2.46521E 02	1.20246E 02	2.71917E 02	151.814 DEG
1 2	3.74423E 01	8.34137E 01	9.14018E 01	65.826 DEG
1 3	-7.24402E 01	-1.10446E 01	7.36598E 01	-169.559 DEG
1 4	1.74680E 02	-3.67462E 01	1.78994E 02	-11.880 DEG
1 5	-9.34674E 02	9.54470E 01	9.38535E 02	174.169 DEG
2 1	-2.53771E 01	1.55984E 01	2.96179E 01	148.220 DEG
2 2	-1.09626E 02	6.86261E 01	1.29335E 02	147.953 DEG
2 3	-1.33068E 02	-8.97468E 01	1.60753E 02	-146.862 DEG
2 4	6.86850E 01	7.29145E 01	1.00171E 02	46.711 DEG
2 5	-1.40450E 02	8.69328E 00	1.40719E 02	176.458 DEG
3 1	-1.78118E 01	2.95548E 00	1.80554E 01	178.579 DEG
3 2	4.46499E 01	5.79932E 01	7.31903E 01	52.407 DEG
3 3	4.37861E 01	1.57705E 02	1.63671E 02	74.483 DEG
3 4	-6.76632E 01	-7.04962E 01	9.77140E 01	-133.825 DEG
3 5	-3.93198E 01	1.10566E 01	4.08447E 01	164.294 DEG
4 1	7.93326E 01	-3.15745E 01	8.53851E 01	21.783 DEG
4 2	-7.60644E 01	-3.43043E 01	8.34421E 01	-155.725 DEG
4 3	6.19323E 01	-1.18942E 02	1.18944E 02	-89.782 DEG
4 4	-1.19028E 02	1.10094E 02	1.62137E 02	137.233 DEG
4 5	2.61463E 02	-1.03344E 01	2.61667E 02	-2.263 DEG
5 1	-1.28417E 01	3.01741E 00	1.31914E 01	166.777 DEG
5 2	-2.74901E 00	-1.26669E 01	1.29617E 01	-182.245 DEG
5 3	6.18284E 01	-2.64710E 01	6.72567E 01	-23.178 DEG
5 4	-8.15376E 01	3.06784E 01	8.71180E 01	159.381 DEG
5 5	1.96189E 01	3.88229E 01	4.34985E 01	63.191 DEG

# 5.5 PROGRAM LISTING

```

S      FORTRAN NLIST00,DECK                                SUP/0210
S      INCLUDE IRIF                                          SUP/0220
CNR19  DRIV                                                  SUP/0230
COMPLEX CZERO,VPIC,SS,DC,U,PHIW,SPHI,PHI,PHITE,DPHI,FXF    SUP/0240
COMMON/C1/KROX(2000),XE(5),YE(3),AG(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS SUP/0250
COMMON/C2/AS,FMACH,FMACH(6),WFREQ,FREQ(10),NMODE,NSURF,LVPIC,SSVPSUP/0260
COMMON/C3/CI(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28) SUP/0270
COMMON/C4/VPIC(1275),SS(2000),DU(28,2),U(10,10,3),PHIW(50),SPHI SUP/0280
COMMON/C5/MOR(51),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TP1,U    SUP/0290
COMMON/C6/X,Y,DX,DY,EH,EK,EKR,EP,EP,NB,NBUX,KODE,MODE,NBW,NBT    SUP/0300
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAJ,QAN,IFR,TWLSUP/0310
COMMON/C8/RND                                                  SUP/0320
1 CALL DAIN                                                  SUP/0330
DO 1000 MACI=1,FMACH                                          SUP/0340
FM=FMACH(MACI)                                                SUP/0350
IF (FM.LT.1.1) GO TO 1000                                     SUP/0360
CALL C00L                                                    SUP/0370
TOR = TWL/BETA                                               SUP/0380
CALL POUT(1)                                                  SUP/0390
U = AS*FM                                                    SUP/0400
TPU = TP1/U                                                  SUP/0410
RFM=DX*(FM/EPJA)*2                                           SUP/0420
DO 500 IFR=1,NFR=0                                           SUP/0430
EK=IFR-Q1IFR)*TPU                                           SUP/0440
EKR = EK*RFM                                                 SUP/0450
EKR = EK*X1/2.0                                              SUP/0460
CALL CAPI                                                    SUP/0470
IF (VPIC.NE.0) CALL POUT(2)                                  SUP/0480
ARG=EK*DX                                                    SUP/0490
FXF=CMPLX(COS(ARG),-SIN(ARG))                                SUP/0500
DO 500 MODE=1,NMODE                                          SUP/0510
DO 10 J=1,50                                                 SUP/0520
10 J0(J,1)=CZERO                                             SUP/0530
IF (NF(MODE,1).EQ.1) GO TO 210                               SUP/0540
X=0.5*DX                                                     SUP/0550
NR=1                                                         SUP/0560
IF (SSVP.NE.0) CALL POUT(3)                                  SUP/0570
DO 200 NP=1,NR=0                                             SUP/0580
KD = KROX(NP)                                                SUP/0590
NS = 1                                                       SUP/0600
GO TO (70,60,70,60,60,70,70),KD                             SUP/0610
60 NS = 2                                                     SUP/0620
70 MH = MOR(NP)                                              SUP/0630
Y=0.0                                                        SUP/0640
DO 100 MP=1,MH                                              SUP/0650
MP = MP                                                       SUP/0660
KODE=(KROX(NP))                                              SUP/0670
SPHI=CZERO                                                  SUP/0680
IF (MP.GT.1) CALL PHIE                                       SUP/0690
SPHI=SPHI*DY                                                 SUP/0700
PHI=CZERO                                                    SUP/0710
GO TO (40,40,40,40,40,20,30),KODE                             SUP/0720
20 SPHI=SPHI-PHIE(1P)                                       SUP/0730
PHI=PHIW(MP)                                                 SUP/0740
PHIW(MP)=PHIW(MP)*FXF                                       SUP/0750
GO TO 50                                                     SUP/0760
30 IF (KD.EQ.6) GO TO 40                                     SUP/0770
50 SS(NR)=-SPHI/VPIC/DY                                       SUP/0780
GO TO 90                                                     SUP/0790
40 CALL WASH                                                  SUP/0800

```

IF(KD.LT.6) SS(NB) = SS(NB)-ARLETOB*(SS(NB)+SPHI/VPIC/DY)	SUP70810
IF(KODE.GE.6) GO TO 90	SUP70820
PHI=SPHI+SS(NB)*VPIC*DY	SUP70830
IF(KODE.EQ.3) PHIW(MP)=PHI*EXF	SUP70840
IF(NP.EQ.NBOX-1) PHIW(MP)=PHI	SUP70850
IF(NP.EQ.NBOX) PHIE=PHI+(PHI-PHIW(MP))*DXE(5)	SUP70860
CALL DQIJ	SUP70870
90 IF(LSSVP.NE.0) CALL PJUT(4)	SUP70880
NB = NB + 1	SUP70890
KD = KODE	SUP70900
100 Y=Y+DY	SUP70910
200 X=X+DX	SUP70920
210 DO 400 MO=1,NMODE	SUP70930
DO 300 NS=1,NSURF	SUP70940
Q(MODE,MO,NS)=CZERO	SUP70950
NTM=NT(MO,NS)	SUP70960
DO 300 N=1,NT	SUP70970
300 Q(MODE,MO,NS)=Q(MODE,MO,NS)+C0(MO,N,NS)*DQ(N,NS)	SUP70980
Q(MODE,MO,3) = CZERO	SUP70990
400 Q(MODE,MO,3)=Q(MODE,MO,1)+Q(MODE,MO,2)	SUP71000
500 CONTINUE	SUP71010
QF = 2.0*DX*DY*RHO	SUP71020
DO 600 NS=1,3	SUP71030
CALL POUT(6)	SUP71040
DO 700 J=1,NMODE	SUP71050
DO 700 K=1,NMODE	SUP71060
QR = QF*REAL(Q(K,J,NS))	SUP71070
QI = QF*AIMAG(Q(K,J,NS))	SUP71080
QAR=SQRT(QI*QI+QR*QR)	SUP71090
QAN=0.0	SUP71100
IF(QAR.NE.0.0) QAN=57.29578*ATAN2(QI,QR)	SUP71110
700 CALL POUT(7)	SUP71120
IF(NSURF.EQ.1) GO TO 900	SUP71130
800 CONTINUE	SUP71140
900 CONTINUE	SUP71150
1000 CONTINUE	SUP71160
GO TO 1	SUP71170
END	SUP71180
\$ FORTRAN NLST00,DECK	SUP71190
\$ INCODE I8PF	SUP71200
CHAIN DAIN	SUP71210
SUBROUTINE DAIN	SUP71220
COMMON/C1/K,DX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS	SUP71230
COMMON/C2/AS,FMACH,FNACH(6),NREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVP	SUP71240
COMMON/C3/C0(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)	SUP71250
COMMON/C6/X,Y,DX,DY,FM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBS,NBT	SUP71260
COMMON/C8/RHO	SUP71270
READ(5,11) (XF(I),I=1,5)	SUP71280
READ(5,11) (YE(I),I=1,3),AS,RHO	SUP71290
RHO = RHO/1000.0	SUP71300
READ(5,12) FMACH,NREQ,NMODE,NBW,LVPIC,LSSVP	SUP71310
READ(5,11) (FMACH(I),I=1,NMACH)	SUP71320
READ(5,11) (FREQ(I),I=1,NREQ)	SUP71330
NSURF=0	SUP71340
IF(XE(4).LT.XE(5)) GO TO 10	SUP71350
NSURF=1	SUP71360
XE(4)=XE(3)	SUP71370
XF(5)=XE(3)	SUP71380
10 NTMAX(1)=0	SUP71390
NTMAX(2)=0	SUP71400

```

DO 30 MODE=1,4MODE
DO 30 I=1,NCONF
DO 20 J=1,NTM
20 CO(MODE,J,I)=0.0
  RFAD(5,12)  TM,NFI
  NT(MODE,I)= TM
  NTMAX(I)=MAX0(NTMAX(I),NTM)
  NF(MODE,I)=NFI
30 RE/AL(5,11) (CO(MODE,J,I),J=1,NTM)
11 FORMAT(6E12.8)
12 FORMAT(6I12)
  RETURN
END
$   FORTRAN NLS100,DECK
$   INCODE IRMF
CCONS      CONS
BLOCK DATA
COMPLEX CZERO,VPIG,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,UPHI
COMMON/C3/CO(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)
COMMON/C4/VPIG(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI
COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),IPI,U
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,IWL
COMMON/C8/RND
DATA KC/1,2,4,7,11,16,22,29,37,46,56,67,79,92,106,121,137,154,172,
1191,211,232,254,277,301,326,352,379,407,436,466,497,529,562,596,
2631,657,704,742,781,821,862,904,947,991,1036,1082,1129,1177,1226/,
3FN/0.,1.,0.,2.,1.,0.,3.,2.,1.,0.,4.,3.,2.,1.,0.,5.,4.,3.,2.,1.,0.,
4 6.,5.,4.,3.,2.,1.,0./,IPI/6.2831853/,CZERO/(0.0,0.0)/
DATA KL/1,1,4,2,3,1,4,5,6,1,7,8,9,10,1,11,12,13,14,15,1,16,17,18,
1 19,20,21,1/
END
$   FORTRAN NLS100,DECK
$   INCODE IRMF
CCODE      CODE
SUBROUTINE CODE
COMPLEX CZERO,VPIG,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,UPHI
COMMON/C1/KLOX(2000),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/AL,AMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIG,LSSVPS
COMMON/C3/CO(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)
COMMON/C4/VPIG(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI
COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),IPI,U
COMMON/C6/X,Y,Dx,DY,EM,FK,EKB,EKR,NP,PP,NB,NBOX,KUDE,MODE,NBW,NBT
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,IWL
COMMON/C8/RND
BETA = SQRT((FM * FM)-1.0)
X1 = XF(3) - XF(1)
X2 = XF(3) - XF(2)
X3 = XF(4) - XF(1)
X4 = XF(5) - XF(4)
X5 = XF(5) - XF(1)
Y1 = YE(2) - YE(1)
Y2 = YE(3) - YE(1)
IF(X2.GT.X1.OR.X1.GT.X3.OR.X3.GT.X5.OR.X2.LT.0.0) GO TO 50
IF(Y1.GT.Y2.OR.Y1.LT.0.0) GO TO 50
TWI = 0.0
IF(Y2.NE.Y1) TWI = (X1 - X2) / (Y2 - Y1)
AR(1) = (Y2*(X2+X1) - Y1 * (X2+X1))
AR(2) = Y2*X4+2.0
AR(3) = AR(1) + AR(2)
10 DX = X1/(FL*AT(1BW) -0.5)

```

```

IF (50.0 * DX .GT. X5) GO TO 20
15 NBW = NBW-1
GO TO 10
20 DY = DX/BETA
YN1 = Y1/DY
YN2 = Y2/DY
XNL = YN2 - (X1-X2) / DX
XNT = YN2 + X5/DX
XNLE = X3/DX
XNTE = X5/DX
NBOX = XNTE+0.5
NBS = Y2/DY + 1.0
NBT = X4/DX + 0.5
DXF(1) = 1.0
DXF(2) = 1.0
DXF(3) = 0.5
DXF(4) = AINT(XNLE + 1.5) - XNLE
DXF(5) = XNTE - FLOAT(NBOX-1)
DXF(6) = 0.0
DXE(7) = 0.0
X = 0.5 * DX
NR = 0
DO 40 NP = 1, NBOX
XN = FLOAT(NP) - 0.5
YW = YN2
IF (TWL .GT. 0.0) YW = AMIN1(YW, YN1+XN/(TWL/BETA))
IF (X .GT. XE(2)) GO TO 24
MR = MIN1(AMAX1(YW, XN+YN1), XNT-XN)+1
GO TO 28
24 MR = MIN1(AMAX1(XNL+XN, XN+YN1), XNT-XN)+1
28 MOR(NP) = MR
KODE = 1
IF (NP .EQ. NBW) KODE = 3
IF (NSURF .EQ. 1) GO TO 29
IF (X .GT. X1) KODE = 6
IF (X .GT. X3) KODE = 4
IF (X .GT. X3+DX) KODE = 2
IF (NP .EQ. NBOX) KODE = 5
29 IF (NR+MR .GT. 2000) GO TO 15
NBI(NP) = NR
DO 30 MP = 1, MR
YN = MP-1
NB = NB + 1
IF (YN .GT. YW) KODE = 7
30 KBOX(NB) = KODE
40 X = X+DX
RETURN
50 CALL EXIT
RETURN
END

```

\$ FORTAN HLSTOU,DECK

\$ INCODE IRIF

CCAFI CAFE

SUBROUTINE CAFE

COMPLEX CZERO,VPIC,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,DPHI

DIMENSION P(5),W(5)

COMMON/C4/VPIC(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI

COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U

COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,RP,NB,NBOX,KODE,MODE,NBW,NBT

COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,UR,QI,QAB,QAN,IFR,TWL

SUP71830  
SUP71840  
SUP71850  
SUP71860  
SUP71870  
SUP71880  
SUP71890  
SUP71900  
SUP71910  
SUP71920  
SUP71930  
SUP71940  
SUP71950  
SUP71960  
SUP71970  
SUP71980  
SUP71990  
SUP72000  
SUP72010  
SUP72020  
SUP72030  
SUP72040  
SUP72050  
SUP72060  
SUP72070  
SUP72080  
SUP72090  
SUP72100  
SUP72110  
SUP72120  
SUP72130  
SUP72140  
SUP72150  
SUP72160  
SUP72170  
SUP72180  
SUP72190  
SUP72200  
SUP72210  
SUP72220  
SUP72230  
SUP72240  
SUP72250  
SUP72260  
SUP72270  
SUP72280  
SUP72290  
SUP72300  
SUP72310  
SUP72320  
SUP72330  
SUP72340  
SUP72350  
SUP72360  
SUP72370  
SUP72380  
SUP75050  
SUP72400  
SUP72410  
SUP72420

```

COMMON/CB/RHO
DATA P/0.95308992,0.76923465,0.5,0.23076535,0.34691008/
1  , W/0.11846344,0.23931434,0.28444444,0.23931434,0.11846344/
PI = TPI/2.0
IF(EKB.GT.0.0) GO TO 10
VPIC = (-1.0,0.0)
GO TO 30
10 VPIC = CZERO
DO 20 I = 1,5
  ARG = EKB*P(I)/2.0
  F = -(0.5*ARG/E4)**2
  ZJ = 1.0
  FI = 1.0
  AE = 1.0
  DO 15 K = 1,20
    AE = AE * F/FI**2
    FI = FI + 1.0
    IF(ABS(AE).LE.1.E-5) GO TO 20
15 7J = ZJ + AE
20 VPIC = VPIC - 7J*W(I)*CMPLX(COS(ARG),-SIN(ARG))
30 DO 80 NP = 2,NBOX
  KI = KC(NP)
  KZ = KC(NP+1) - 1
  DO 40 K = KI,KZ
40 VPIC(K) = CZERO
  NU = NP - 1
  DO 60 I = 1,5
    X = FLOAT(NU) - 0.5 + P(I)
    ARG = EKB*X
    PHI = W(I)*CMPLX(-COS(ARG),SIN(ARG))*2.0/PI
    CALL BSLS(ARG/E4,N)
    K = KC(NP)
    DO 70 MP = 1,NU
      EOX = (FLOAT(MP) - 0.5)/X
      C = SQRT(1.0 - EOX**2)
      AF = 2.0*ATAN(EOX/(1.0 + C))
      S = 2.0*EOX*C
      C = 2.0*C*C - 1.0
      SO = 0.0
      VIN = BSL*AF
      F = 1.0
      FI = 1.0
      DO 50 L = 1,N
        VIN = BSL(L+1)*S/FI - VIN
        SN = 2.0*S*C - SO
        SO = S
        S = SN
        F = -F
50 FI = FI + 1.0
      DPHI = PHI*VIN*F
      VPIC(K) = VPIC(K) + DPHI
      VPIC(K+1) = VPIC(K+1) - DPHI
      IF(MP.EQ.1) VPIC(K) = VPIC(K) + DPHI
70 K = K + 1
80 VPIC(K) = VPIC(K) + PI*BSL*PHI/2.0
  RETURN
END
$   FORTRAN NLSTOU,DECK
$   INCOEF  IB:F
CBSLS      BSLS

```

SUP72430  
 SUP72440  
 SUP72450  
 SUP72460  
 SUP72470  
 SUP72480  
 SUP72490  
 SUP72500  
 SUP72510  
 SUP72520  
 SUP72530  
 SUP72540  
 SUP72550  
 SUP72560  
 SUP72570  
 SUP72580  
 SUP72590  
 SUP72600  
 SUP72610  
 SUP72620  
 SUP72630  
 SUP72640  
 SUP72650  
 SUP72660  
 SUP72670  
 SUP72680  
 SUP72690  
 SUP72700  
 SUP72710  
 SUP72720  
 SUP72730  
 SUP72740  
 SUP72750  
 SUP72760  
 SUP72770  
 SUP72780  
 SUP72790  
 SUP72800  
 SUP72810  
 SUP72820  
 SUP72830  
 SUP72840  
 SUP72850  
 SUP72860  
 SUP72870  
 SUP72880  
 SUP72890  
 SUP72900  
 SUP72910  
 SUP72920  
 SUP72930  
 SUP72940  
 SUP72950  
 SUP72960  
 SUP72970  
 SUP72980  
 SUP72990  
 SUP73000  
 SUP73010  
 SUP73020



```

SUBROUTINE BSLS(ARG,N)
COMMON/C5/HDR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U
COMMON/C8/RHO
DO 1 I=1,20
1 BSL(I) = 0.0
ASQ = ARG**2
IF(ASQ.LT.0.01) GO TO 50
N = MIN1(17.0,(ARG + 10.0))
F = 2*N + 4
BSL(N+2) = (4.0*F*(F-1.0)/ASQ-(F-1.0)/F)*0.3E-30
PF = 0.0
J = 0
DO 10 I = J,N
M = N - I + 1
F = 2*M + 1
BSL(M) = (4.0*(F-1.0)/ASQ-1.0/F-1.0/(F-2.0))*BSL(M+1)-BSL(M+2)/F
10 PF = PF + 2.0*(F-2.0)*BSL(M+1)
PF = PF + BSL(1)
F = 0.0
IF(ABS(PF).GT.1.0) F = ABS(PF)*1.E-10
N = N + 2
DO 30 I = 1,N
IF(F.GE.ABS(BSL(I))) GO TO 20
BSL(I) = BSL(I)/PF
GO TO 30
20 BSL(I) = 0.0
30 CONTINUE
DO 40 I = 1,N
IF(ABS(BSL(N)).GT.1.0 E-7) RETURN
40 N = N - 1
RETURN
50 BSL(2) = -0.125*ASQ
BSL(1) = 1.0 - 2.0*BSL(2)
N = 2
RETURN
END

```

\* FORTRAN NESTOU,DECK

\* INCODE IBMF

CARLE ARLE

FUNCTION ARLE(TOB)

COMMON/C1/KBOX(200.0),XF(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS

COMMON/C6/X,Y,DX,DY,EM,EK,EKB,ENR,NP,PP,NB,NBOX,KODE,MODE,NBW,NBT

COMMON/C8/RHO

IF(X-0.5\*DX.GE.X1-X2) GO TO 10

YT = (Y-Y1)/DY+0.5-(X/DX-0.5)/TOB

XR = YT\*TOB

YB = AMAX1(0.0,AMIN1(1.0,YT-1.0/TOB))

YT = AMIN1(1.0,AMAX1(0.0,YT))

XL = AMAX1(0.0,AMIN1(1.0,XR-TOB))

XR = AMIN1(1.0,AMAX1(0.0,XR))

ARLE = AMAX1(0.5\*(YT\*(XR+XL)+YB\*(XR-XL)),0.0)

IF(MP.EQ.1) ARLE = 2.0\*ARLE

RETURN

10 ARLE = AMIN1(1.0,AMAX1(0.0,(Y-Y2)/DY+0.5))

RETURN

END

\* FORTRAN NESTOU,DECK

\* INCODE IBMF

CPHIB PHIB

SUBROUTINE PHIB

SUP73030  
 SUP73040  
 SUP73050  
 SUP73060  
 SUP73070  
 SUP73080  
 SUP73090  
 SUP73100  
 SUP73110  
 SUP73120  
 SUP73130  
 SUP73140  
 SUP73150  
 SUP73160  
 SUP73170  
 SUP73180  
 SUP73190  
 SUP73200  
 SUP73210  
 SUP73220  
 SUP73230  
 SUP73240  
 SUP73250  
 SUP73260  
 SUP73270  
 SUP73280  
 SUP73290  
 SUP73300  
 SUP73310  
 SUP73320  
 SUP73330  
 SUP73340  
 SUP73350  
 SUP73360  
 SUP73370  
 SUP73380  
 SUP73390  
 SUP73400  
 SUP73410  
 SUP73420  
 SUP73430  
 SUP73440  
 SUP73450  
 SUP73460  
 SUP73470  
 SUP73480  
 SUP73490  
 SUP73500  
 SUP73510  
 SUP73520  
 SUP73530  
 SUP73540  
 SUP73550  
 SUP73560  
 SUP73570  
 SUP73580  
 SUP73590  
 SUP73600  
 SUP73610  
 SUP73620

COMPLEX CZERO,VPIC,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,DPHI	SUP73630
COMMON/C4/VPIC(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI	SUP75050
COMMON/C5/MOB(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U	SUP73650
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,MP,MP,NB,NBOX,KODE,MODE,NBW,NBT	SUP73660
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL	SUP73670
COMMON/C8/RHO	SUP73680
DO 20 I=2,NP	SUP73690
NU=NP-I+1	SUP73700
JL=MAX0(1,MP-I+1)	SUP73710
JR=MIN0(MOB(NU),MP+I-1)	SUP73720
NJ=NBL(NU)+JL	SUP73730
DO 20 J=JL,JR	SUP73740
K=KC(I)+IABS(MP-J)	SUP73750
DPHI=VPIC(K)	SUP73760
IF (J.GT.1-MP+1.OR.J.EQ.1) GO TO 10	SUP73770
K=KC(I)+MP+J-2	SUP73780
DPHI=DPHI+VPIC(K)	SUP73790
10 SPHI=SPHI+DPHI*SS(NJ)	SUP73800
20 NJ=NJ+1	SUP73810
RETURN	SUP73820
END	SUP73830
\$     FORTRAN NLSTOU,DECK	SUP73840
\$     INCODE IBMF	SUP73850
CDCIJ     DUIJ	SUP73860
SUBROUTINE DUIJ	SUP73870
COMPLEX CZERO,VPIC,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,DPHI	SUP73880
COMMON/C1/KINDX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS	SUP73890
COMMON/C3/CO(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)	SUP73900
COMMON/C4/VPIC(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI	SUP75050
COMMON/C5/MOB(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U	SUP73920
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,MP,MP,NB,NBOX,KODE,MODE,NBW,NBT	SUP73930
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL	SUP73940
COMMON/C8/RHO	SUP73950
NTM = NTMAX(NS)	SUP73960
DPHI=PHI	SUP73970
IF (MP.EQ.1) DPHI=0.5*DPHI	SUP73980
CON = U*DXE(KODE)	SUP73990
DO 20 K=1,NIM	SUP74000
KK=AB(K)	SUP74010
20 DQ(K,NS) = DQ(K,NS) + DPHI*CON*CMPLX(PXY(KK)*FN(K),-EK*PXY(K))	SUP74020
IF(KODE.NE.3) GO TO 50	SUP74030
DO 30 K = 1,NTM	SUP74040
30 DQ(K,1) = DQ(K,1) -U*DPHI*PXY(K)/DX	SUP74050
ARG = EK*(X3 - X1)	SUP74060
DPHI = -DPHI*CMPLX(COS(ARG),-SIN(ARG))	SUP74070
XL = 0.0	SUP74080
CALL QEGE	SUP74090
50 IF(KODE.NE.5) RETURN	SUP74100
XL = X4	SUP74110
IF(MP.EQ.1)PHITE = 0.5*PHITE	SUP74120
DPHI = PHITE	SUP74130
CALL QEGE	SUP74140
RETURN	SUP74150
END	SUP74160
\$     FORTRAN NLSTOU,DECK	SUP74170
\$     INCODE IBMF	SUP74180
CQEGE     QEGE	SUP74190
SUBROUTINE QEGE	SUP74200
COMPLEX CZERO,VPIC,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,DPHI	SUP74210
COMMON/C4/VPIC(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI	SUP75050

COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TP1,U	SUP74230
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBW,NBT	SUP74240
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL	SUP74250
COMMON/C8/RHO	SUP74260
PX=1.0/DX	SUP74270
IF(XL.EQ.0.0) GO TO 30	SUP74280
YX=Y/XL	SUP74290
K=1	SUP74300
DO 20 N=1,7	SUP74310
PY=PX	SUP74320
DO 10 M=1,N	SUP74330
DQ(K,2) = DQ(K,2) - U*DPHI*PY	SUP74340
IF(K.EQ.NTM) RETURN	SUP74350
K=K+1	SUP74360
10 PY=PY*YX	SUP74370
20 PX=PX*XL	SUP74380
RETURN	SUP74390
30 K=0	SUP74400
DO 40 N=1,7	SUP74410
K=K+N	SUP74420
IF(K.GT.NTM) RETURN	SUP74430
DQ(K,2) = DQ(K,2) - U*DPHI*PX	SUP74440
40 PX=PX*Y	SUP74450
RETURN	SUP74460
END	SUP74470
* FORTTRAN NLSTOD,DECK	SUP74480
* INCODE IBMF	SUP74490
CWASH WASH	SUP74500
SUBROUTINE WASH	SUP74510
COMPLEX CZERO,VPIC,SS,DQ,Q,PHIW,SPHI,PHI,PHITE,DPHI	SUP74520
COMMON/C1/KBOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS	SUP74530
COMMON/C3/CO(10,28,2),NT(10,2),NF(10,2),NTMAX(2),PXY(28),FN(28)	SUP74540
COMMON/C4/VPIC(1275),SS(2000),DQ(28,2),Q(10,10,3),PHIW(50),SPHI	SUP75050
COMMON/C5/MOR(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TP1,U	SUP74560
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBW,NBT	SUP74570
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTM,K,J,QR,QI,QAB,QAN,IFR,TWL	SUP74580
COMMON/C8/RHO	SUP74590
XP = X	SUP74600
IF(NS.EQ.2) XP = X - X3	SUP74610
PXY = 1.0	SUP74620
DO 10 N = 2,28	SUP74630
10 PXY(N) = 0.0	SUP74640
TM = NTMAX(NS)	SUP74650
ID = SQRT(2.0*TM) - 0.5	SUP74660
IF(ID.EQ.0) GO TO 60	SUP74670
K = 1	SUP74680
IF(XP.EQ.0.0) GO TO 40	SUP74690
YX = Y/XP	SUP74700
PX = XP	SUP74710
DO 30 N = 1,10	SUP74720
K = K + 1	SUP74730
PXY(K) = PX	SUP74740
DO 20 M = 1,N	SUP74750
K = K + 1	SUP74760
20 PXY(K) = PXY(K-1)*YX	SUP74770
30 PX = PX*XP	SUP74780
GO TO 60	SUP74790
40 PX = 1.0	SUP74800
DO 50 N = 1,10	SUP74810
PXY(K) = PX	SUP74820

```

K = K + N + 1
50 PX = PX*Y
60 NTH = NT(MODE,NS)
Z = CO(MODE,1,NS)
DZ = 0.0
IF(NTH.EQ.1) GO TO 80
DO 70 K = 2,NTH
7 = Z + PXY(K)*CO(MODE,K,NS)
KK = KL(K)
70 DZ = DZ + PXY(KK)*CO(MODE,K,NS)*FN(K)
80 SS(NB) = U*CMPLX(DZ,EK*2)
RETURN
END
S      FORTRAN NLSTON,DECK
CROUT  POUT
SUBROUTINE POUT(IND)
COMPLEX CZERO,VPIC,SS,DU,Q,PHIW,SPHI,PHI,PHITE,DPHI
DIMENSION CARDS (25,50)
*****
DIMENSION SW(5,6),SURF(2,3),COD(7),C(50)
COMMON/C1/KPOX(2000),XE(5),YE(3),AR(3),X1,X2,X3,X4,Y1,Y2,BETA,NBS
COMMON/C2/AS,NMACH,FMACH(6),NFREQ,FREQ(10),NMODE,NSURF,LVPIC,LSSVPS
COMMON/C3/CO(10,28,2),NI(10,2),NF(10,2),NTHAX(2),PXY(28),FN(28)
COMMON/C4/VPIC(1275),SS(2000),DU(28,2),Q(10,10,3),PHIW(50),SPHI
COMMON/C5/MOB(50),NBL(50),KC(50),KL(28),BSL(20),DXE(7),TPI,U
COMMON/C6/X,Y,DX,DY,EM,EK,EKB,EKR,NP,MP,NB,NBOX,KODE,MODE,NBW,NBT
COMMON/C7/CZERO,PHI,PHITE,DPHI,XL,NS,NTH,K,J,QR,Q1,QAB,QAN,IFR,TWLS
COMMON/C8/RHO
DATA (SW(1,I),I=1,6)/26HMAP OF MACH BOX OVERLAY ON,
1      26HWING, TAIL, AND DIAPHRAGM ,
2      26H      (S) - WING ,
3      26H      (S) - TAIL ,
4      26H      (.) - WAKE ,
5      26H      (.) - DIAPHRAGM /
DATA (SURF(1,I),I=1,3)/8HWING ,8HTAIL ,11HWING + TAIL /
DATA COD/1HS,1HS,1HS,1HS,1HS,1H,,1H./
GO TO (10,20,30,40,50,60,70),IND
10 WRITE(6,11)FM,AS,RHO,XE(1),XE(4),X1,X4,Y1,Y2,Y2,Y2,X2,X4,AR(1),
1 AR(2),NBW,NBT,NBS,NBS
11 FORMAT(1H1////////30X,43HMAC/NAA MISSILE SUPERSONIC AIRLOADS PROGRAMS
1 ///37X,30HFLIGHT CONDITIONS AND GEOMETRY/1H0//15X, 13HMACH NUMBERS
2 =,F8.5,4X,16HSPEED OF SOUND =F10.3,4H L/T,4X,4HRHO=,E14.8//1H0/
X54X,4HWING,18X,
3 4HTAIL//22X,16HL.F. STATION (L),2F22.3//22X,16HROOT CHORD (L),
4 2F22.3// 22X,16HL.F. SPAN (L),2F22.3//22X,16HT.E. SPAN (L),
5 2F22.3// 22X,16HTIP CHORD (L),2F22.3//22X,16HTOTAL AREA (L*L),
6 2F22.3// 22X,16HCHORDWISE BOXES ,I19,I22//22X,
/16HSPANWISE BOXES ,I19,I22)
WRITE(6,12)NBOX,DX,DY
12 FORMAT(1H0//,11X,23HTOTAL CHORDWISE BOXES =,I3, 5X,11HBOX CHORD =,
1 1P1E12.5,2H L, 5X,10HBOX SPAN =,1P1E12.5,2H L/ )
WRITE(6,91)
NB = 1
DO 17 NP = 1,NBOX
MB = MOB(NP)
IF(MB.GT.50) GO TO 800
DO 13 MP = 1,MB
K = KBOX(NB)
C(MP) = COD(K)
13 NB = NB + 1
IF(NP.GT.6) GO TO 15

```

```

      WRITE(6,14) (SH(I,HP), I=1,5), (C(HP), HP=1,HB)
14  FORMAT(10X,5A6,50A1)
      GO TO 17
15  WRITE(6,16) (C(HP), HP=1,HB)
16  FORMAT(40X,50A1)
17  CONTINUE
      GO TO 1000
800  WRITE(6,801)
801  FORMAT(9X,52HWHEN MOB EXCEEDS 50 THE MAP PRINTING IS DISCONTINUED
17/1H0,48H          CALCULATIONS PROCEED IN NORMAL MANNER          )
      GO TO 1000
20  WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
      WRITE(6,21) EM, EKB
21  FORMAT(1H ,28X,48HPLANAR VELOCITY POTENTIAL INFLUENCE COEFFICIENTS
1 /1H0,30X,10HACH NO. =,F8.5,10X, 6HKBAR =,F9.5/1H0,13X,1H1,5X,1HJSUP75560
2 10X,5HNUBAR,5X,5HMUBAR,11X,14HREAL VPIC(I,J),8X,14HIMAG VPIC(I,J)SUP75570
3 /1H )
      K = 0
      DO 22 I = 1, NBOX
      DO 22 J = 1, 1
      BARNU = I - 1
      BARMU = J - 1
      K=K+1
22  WRITE(6,23) I, J, BARNU, BARMU, VPIC(K)
23  FORMAT(9X,216,4X,2F10.1,2X,1P2E22.5)
      GO TO 1000
30  WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
      WRITE(6,31) MODE
31  FORMAT(1H ,21X, 59HUPPER VELOCITY POTENTIALS AND SOURCE STRENGTHSSUP75700
1 FOR MODE NO.13/1H0,9X,1HN,6X,1HM,5X,2HNB,7X,10HR PHI(N,M),7X,10HSUP75710
2 PHI(N,M)10X,9HR SS(N,M),8X,9HII SS(N,M)/1H )
      GO TO 1000
40  WRITE(6,41) HP, MP, HB, PHI, SS(NB)
41  FORMAT(4X,317,122E17.5,3X,1P2E17.5)
      GO TO 1000
60  IF(NS.EQ.3) GO TO 100
50  WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
51  FORMAT(1H1,33X,44HMISSILE SUPERSONIC AIRLOADS PROGRAM (CONT=D)// SUP75790
X1H0
1 8X,27HOSCILLATORY FREQUENCY (CPS),F12.5,14X,12,25H BOXES IN CHORDSUP75810
2 DIRECTION /1H0,8X,30HREDUCED FREQUENCY (SEMI CHORD),F9.5,14X, SUP75820
3 23HFREE STREAM MACH NUMBER,F9.3,/1H )
      WRITE(6,101) SURF(1,NS)
101  FORMAT(28X,45HINPUT MODE SHAPE POLYNOMIAL COEFFICIENTS FOR ,A6/ SUP75850
1 22X,62HREFERENCED TO THE SURFACE LEADING EDGE-CENTERLINE INTERSECSUP75860
2TION //2X,4HMODE,20X, 7HCoeffs.)
      DO 102 I=1, NMODE
      NTM=NT(I,NS)
102  WRITE(6,103) I, (CU(I,J,NS), J=1,NTM)
103  FORMAT(1H0,14,4X,1P7E13.4/(9X,1P7E13.4))
100  WRITE(6,51) FREQ(IFR), NBOX, EKR , EM
      WRITE(6,61) (SURF(I,NS), I=1,2)
61  FORMAT(1H ,35X,23HGENERALIZED FORCES FOR ,2A6/1H0,6X,4HDEF L,3X, SUP75940
1 4HLOAD,10X,9HREAL PART,10X,9HIMAG PART,10X,9HABS VALUE,10X, SUP75950
2 11HPHASE ANGLE //)
      GO TO 1000
70  WRITE(6,71) J, K, QR, Q1, QAB, QAN
      IF (NSURF.EQ. 1) GO TO 632
      IF (NS.NE.3) GO TO 1000
632  KKK=2*NMODE

```

\*\*\*\*\*

```

NNN=2*K
NNNN=NNN-1
CARDS(J,NNNN)=QR
CARDS(J,NNN)=QI
IF (J.NE.NMODE) GO TO 1000
IF (K.NE.NMODE) GO TO 1000
PUNCH 6969, ((CARDS(I,J),JJ=1,KKK), I=1,NMODE)
6969 FORMAT(6E12.5)
71 FORMAT(1H0,19,17,2X,1P3E19.5,0PF16.3,4H DE8)
91 FORMAT(1H1,30X,44HMISSILE SUPERSONIC AIRLOADS PROGRAM (CONT-D))//
1000 RETURN

```

```

*****
*****
*****
*****
*****
*****
*****
*****
SUP75990
SUP76000
SUP76010

```

## REFERENCES

1. Bisplinghoff, R. L., Ashley, H., Halfman, R. L., *Aeroelasticity*, Addison - Wesley Publishing Co. Inc., 1955.
2. Bisplinghoff, R. L., Ashley, H., *Principles of Aeroelasticity*, John Wiley and Son Inc., 1968.
3. Gravitz, S. I., "Analytical Procedure for Orthogonalization of Experimentally Measured Modes", *Journal of the Aero Space Sciences*, Vol. 25, No. 11, Nov. 1958, pp. 721-722.
4. McGrew, J., "Orthogonalization of Measured Modes and Calculation of Influence Coefficients", *AIAA Journal*, Vol. 7, No. 4, April 1969, pp. 774-776.
5. Vivian, H. T. and L. V. Andrew, "Unsteady Aerodynamics for Advanced Configurations, Part I - Application of the Subsonic Kernel Function to Nonplanar Lifting Surfaces", *Air Force Flight Dynamics Laboratory Report FDL-TDR-64-152, Part I* (1965).
6. Rodemich, E. R. and L. V. Andrew, "Unsteady Aerodynamics for Advanced Configurations, Part II - A Transonic Box Method for Planar Lifting Surfaces", *Air Force Flight Dynamics Laboratory Report FDL-TDR-64-152, Part II* (1964).
7. Moore, M. T. and L. V. Andrew, "Unsteady Aerodynamics for Advanced Configurations, Part IV - Application of the Supersonic Mach Box Method to Intersecting Planar Lifting Surfaces", *Air Force Flight Dynamics Laboratory Report FDL-TDR-64-152, Part IV* (1965).
8. Garrick, I. E. and S. I. Rubinow, "Theoretical Study of Air Force on an Oscillating or Steady Thin Wing in a Supersonic Main Stream", *NACA Report 872* (1948).
9. Hsu, P. T., "Calculation of Pressure Distributions for Oscillating Wings of Arbitrary Planform in Subsonic Flow by the Kernel Function Method, Part I", *MIT Aeroelasticity and Structures Research Laboratory Technical Report 641* (1957).
10. MSD MAV 2.21.10-1, "Development/Qualification Test Report - Modal Vibration," Data Item T-119, 15 Dec. 1969.
11. S. Pines, K. Dugundji, and J. Neuringer, "Aerodynamic Flutter Derivatives for a Flexible Wing with Supersonic and Subsonic Leading Edge," *Journal of the Aeronautical Sciences*, Volume 22, No. 10, October 1955.